

Checking In 3/21/2024

Wednesday, March 27, 2024 2:09 PM



Andrews, Edward S <edward.s.andrews@wv.gov>

Checking In

1 message

Wood, Katie <katie.wood@tetrattech.com>
To: Edward Andrews <edward.s.andrews@wv.gov>

Thu, Mar 21, 2024 at 1:23 PM

Hey Ed,

Just wanted to check in and see if you needed anything further for Empire.

Thanks,

Katie

Katie Wood* | Environmental Scientist
Direct **+1 (740) 298-9062** | Mobile **+1 (304) 559-9980** | katie.wood@tetrattech.com
Formerly Katie Pugh, please note name change
Tetra Tech | *Leading with Science®* | OGA
47443 National Rd Suite 3 | St. Clairesville, OH 43950 | tetrattech.com

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Further Discussion 3/11/2024

Wednesday, March 27, 2024 2:08 PM



Andrews, Edward S <edward.s.andrews@wv.gov>

Re: Empire Discussion

1 message

Andrews, Edward S <edward.s.andrews@wv.gov>

Mon, Mar 11, 2024 at 1:26 PM

To: "Farley R. Wood, P.E." <fwood@empirede.com>

Cc: "Wood, Katie" <katie.wood@tetrattech.com>, Malcolm Kingston <design@technotherm.co.za>

Thanks for the follow up with my concerns about the process.

I will provide either a my understanding of the decay of PVC and formation of HCl with recovery or an illustration/flow diagram with which we can have a discussion about.

Thanks
Ed

On Mon, Mar 11, 2024 at 1:15 PM Farley R. Wood, P.E. <fwood@empirede.com> wrote:

Ed,

See my comments below:



Farley R. Wood, P.E.
Vice President of Engineering


Main Office (304) 935-5851
Mobile: (304) 650-2023
Teams: [Click Here](#)

fwood@empirede.com
www.empirediversifiedenergy.com

From: Wood, Katie <katie.wood@tetrattech.com>
Sent: Friday, March 8, 2024 3:15 PM
To: Farley R. Wood, P.E. <fwood@empirede.com>
Subject: FW: Empire Discussion

You don't often get email from katie.wood@tetrattech.com. [Learn why this is important](#)

From: Andrews, Edward S <edward.s.andrews@wv.gov>
Sent: Friday, March 8, 2024 3:10 PM
To: Wood, Katie <katie.wood@tetrattech.com>
Subject: Re: Empire Discussion

 **CAUTION:** This email originated from an external sender. Verify the source before opening links or attachments.



Katie,

I have looked over the latest request to my questions.

Some things are making sense(e.g, formation of HCl from the pyrolysis unit).

However, I am still a little confused on how the gaseous HCl in the synthetic gas is going to be stripped out with the gas cleaning trains without a significant amount of water being entrained into the cleaned synthetic gas stream.

The Cl gas will be liberated in the pre-pyrolysis unit and removed before the feed enters the pyrolysis unit, where the syngas is produced.

I saw that there was some HCl estimated from the scrubber in the revised application but I did not receive any attachments in your February 21 email (tanks/HCl calculations).

Katie will forward to you.

Here are some of my concerns/questions that I still have:

A)1) Make up the PVC in the plastic feedstock. At 100% PVC, about 15.5 gallons per minute of 20% HCl could potentially be produced. At this rate, the storage capacity would be exceeded in one day.

We cannot run 100% PVC feed to the plant. We are limited to 15%, and should produce a maximum of 5,500 gallons per day of HCl.

We also have the option of running less than 15% to reduce HCl production, or not run any PVC to effectively stop HCl production.

A)2) Operating temperature range of the pyrolysis unit.

The pre-pyrolysis units operating temperature is 320° C (608° F). The operating temperature of the pyrolysis unit is 830° C (1,526° F).

A)3) Will oils/tars still be produced? One of the references in the provided paper noted the formation of methane, ethane, ethyne, 1-butane, hydrogen, chlorine, and benzene, which are in the form of C_nH_m. None of these compounds

are close to C14

Oils/tars will be produced. We have an oil/water separator on the HCl circuit, and a larger oil/water separator on each of the three gas cleanup trains.

The collected oil/tars are pumped to a central collection tank where the product is used as fuel in the combustion chamber of the pyrolysis units.

B) I am assuming the gas cleaning trains are going to be used to extract the gaseous HCl out of the synthetic gas. How does EGG plan on doing this and what properties are going to be monitored?

I am envisioning that the scrubber would be blown down once the circulating water reached a HCl conc of 20% or sg of 1.1. This needs to be spelled out.

The Cl gas will be collected and removed from the system prior to the generation of syngas.

C) Venting the HCl scrubber to the RTO might be the simplest approach. Operating pressures and water/HCl carryover might adversely affect the life and performance of the RTO. Please see Note 3 on DWG Poly Scrub Basis 5'x5' scrubber that the vessel is designed for 1.9 SpG Mat'l @ 100 F/Atmos Pressure.

The HCl fumes will pass through the scrubber which is 99% efficient. There will not be any water carryover.

There will be high dilution of the very low concentration HCl fumes returning to the RTO that the designers of the system feel any adverse effects to life cycle or performance would be negligible.

Stipping gaseous HCl with water is going to generate a significant amount of heat energy.

The HCl system has two chiller units included in the circuit. One for the gasses entering the spray tower, and a second for the liquid leaving the tower.

Plus connecting the vent line to the RTO is going to reduce the operating pressure below atmospheric (negative pressure).

That is correct. We want negative pressure from the HCl scrubber to the RTO to prevent leakage.

D) Classification of the plastic feedstock is either a fuel/raw ingredient in accordance with 40 CFR 241.

Good

On Fri, Mar 1, 2024 at 10:23 AM Wood, Katie <katie.wood@tetrattech.com> wrote:

Ed,

We have some answers to your questions below in red. Please let me know if you would like to discuss.

Thanks,

Katie

From: Andrews, Edward S <edward.s.andrews@wv.gov>

Sent: Friday, February 23, 2024 2:24 PM

To: Wood, Katie <katie.wood@tetrattech.com>; Farley Wood <fwood@empirede.com>

Subject: Re: Empire Discussion

⚠ CAUTION: This email originated from an external sender. Verify the source before opening links or attachments. ⚠

Using Chlorine gas and water reaction to produce HCl also produces a by-product of HOCl (hypochlorous acid). <https://www.bing.com/search?q=chlorine+gas+water+reaction&qs=UT&pq=chlorine+gas+water+reaction&sc=10-27&cvid=1D306673308642F9BCEE5D950B9BFB08&FORM=QBRE&sp=1&ghc=1&lq=0> The process does not produce any Chlorine gas, it produces Chloride gas so no HOCL is produced. I have attached a paper provided by Technotherm for futher information

Question is: Will Empire separate hypochlorous acid from the HCl or send it out as it? As per above no HOCL will be produced

Will the emissions of HCl go through a separate release point than the RTO stack? If it is a separate stack, I need the stack id and stack parameters of this point. No all emissions will go through the RTO

Also, I will need the calculations to support your emission estimate of HCl and concentration of HCl in the effluent release to the atmosphere from the production/storage/loading out of HCl. Calculations attached, these were included in the last submittal

Ed

On Thu, Feb 22, 2024 at 1:00 PM Wood, Katie <katie.wood@tetrattech.com> wrote:

Microsoft Teams meeting

Join on your computer, mobile app or room device

[Click here to join the meeting](#)

Meeting ID: 248 808 531 032

Passcode: Gbfah4

[Download Teams](#) | [Join on the web](#)

Or call in (audio only)

+1 213-357-2812,,114016353# United States, Los Angeles

Phone Conference ID: 114 016 353#

[Find a local number](#) | [Reset PIN](#)

[Learn More](#) | [Meeting options](#)

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Edward Andrews, P.E.

Engineer

WVDEP/Division of Air Quality

304-926-0499 Ext 41244

601 57th Street, SE

Charleston, WV 25304

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601 57th Street, SE

Charleston, WV 25304

External Email. Please make sure you trust this sender before clicking on any links or opening attachments. [Learn why this is important](#)

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Edward Andrews, P.E.
Engineer
WVDEP/Division of Air Quality
304-926-0499 Ext 41244
601 57th Street, SE
Charleston, WV 25304

Scrubber Forms 3/11/2024

Wednesday, March 27, 2024 2:05 PM



Andrews, Edward S <edward.s.andrews@wv.gov>

RE: Empire Discussion

1 message

Wood, Katie <katie.wood@tetratech.com>
To: "Andrews, Edward S" <edward.s.andrews@wv.gov>
Cc: Farley R Wood <fwood@empirede.com>

Mon, Mar 11, 2024 at 1:09 PM


Ed,

Attached is the emission control sheet for the scrubber. Farley is pulling together answers for you questions below and will be sending over shortly.

Thanks,

Katie

From: Andrews, Edward S <edward.s.andrews@wv.gov>
Sent: Friday, March 8, 2024 3:10 PM
To: Wood, Katie <katie.wood@tetratech.com>
Subject: Re: Empire Discussion

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A)2) Operating temperature range of the pyrolysis unit.

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Stripping gaseous HCl with water is going to generate a significant amount of heat energy.

Plus connecting the vent line to the RTO is going to reduce the operating pressure below atmospheric (negative pressure).

D) Classification of the plastic feedstock is either a fuel/raw ingredient in accordance with 40 CFR 241.

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Subject: Re: Empire Discussion

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Using Chlorine gas and water reaction to produce HCl also produces a by-product of HOCl (hypochlorous acid). <https://www.bing.com/search?q=chlorine+gas+water+reaction&q=UT&pq=chlorine+gas+water+reaction&sc=10-27&cvid=1D306673308642F9BCEE5D950B9BFB08&FORM=QBRE&sp=1&ghc=1&lq=0> The process does not produce any Chlorine gas, it produces Chloride gas so no HOCL is produced. I have attached a paper provided by Technotherm for further information

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Ed

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Microsoft Teams meeting

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[Click here to join the meeting](#)

Meeting ID: 248 808 531 032

Passcode: Gbfah4

[Download Teams](#) | [Join on the web](#)

Or call in (audio only)

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Phone Conference ID: 114 016 353#

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[Charleston, WV 25304](#)

 **M-3.pdf**
2632K



M-3

Attachment M
Air Pollution Control Device Sheet
(WET COLLECTING SYSTEM-SCRUBBER)

Control Device ID No. (must match Emission Units Table):

Equipment Information

1. Manufacturer: Poly Processing Model No. 5' X 5" Scrubber	2. Method: <input type="checkbox"/> Packed Bed <input type="checkbox"/> Venturi <input type="checkbox"/> Spray Tower <input type="checkbox"/> Cyclone <input type="checkbox"/> Mechanical <input type="checkbox"/> Orifice <input checked="" type="checkbox"/> Other, specify
3. Provide diagram(s) of unit describing capture system with duct arrangement and size of duct, air volume, capacity, horsepower of movers. If applicable, state hood face velocity and hood collection efficiency.	
4. Provide a scale diagram of the scrubber showing internal construction. Please include packing type and size, spray configurations, baffle plates, and mist eliminators.	
5. What type of liquid entrainment eliminators or system will be used? Submit a schematic diagram showing thickness, mesh, and material of construction.	
6. Describe the scrubber's construction material: Polyethylene (XLPE tank with PVC internals and exterior piping. Water with NaOH is added to the vessel above the set level. Vent gas from the HCl tank passes through the gas diffuser where HCl fumes are neutralized before the scrubbed gas is vented from the top.	
7. What will be the power requirements of the collector? Fan NO HP Inlet scrubbing liquid pump: NA HP	
8. What type of fan(s) will be used? Type of fan blade: None Number of blades: None Diameter of blade: None in. Also supply a fan curve for each fan to be used.	
9. Estimated gas pressure drop at maximum flow rate: 1 inches H ₂ O	

Scrubbing Liquor Characteristics

10. Scrubbing Liquor	11. Scrubbing liquor losses (evaporation, etc.): 0.5 gal/1000 ACF gas										
<table border="1"> <thead> <tr> <th>Composition</th> <th>Weight %</th> </tr> </thead> <tbody> <tr> <td>1 Water</td> <td>99</td> </tr> <tr> <td>2 NaOH</td> <td>1</td> </tr> <tr> <td>3</td> <td></td> </tr> <tr> <td>4</td> <td></td> </tr> </tbody> </table>	Composition	Weight %	1 Water	99	2 NaOH	1	3		4		12. Liquor pressure to scrubber: 0.25 PSIA
Composition	Weight %										
1 Water	99										
2 NaOH	1										
3											
4											
	13. Pressure drop through scrubber: 6 in. H ₂ O										
14. Source of liquor (explain): Batch liquid added to tank	15. Liquor flow rates to scrubber: Design maximum: 1,000 gal/min Average expected: 500 gal/min										
16. Describe system to be used to supply liquor to collector: Manual drain and re-fill process											
17. Give the expected solids content of the liquor: No suspended solids will be created. The system will convert HCl gas vapors will react with NaOH to form water (H ₂ O) and salt (NaCl). Water will be changed out well before NaCl concentration reaches saturation.											

18. If the liquor is to be recirculated, describe any treatment performed:	
19. Data for Venturi Scrubber: Throat Dimensions: NA (Specify Units) Throat Velocity: Na ft/sec	20. Data for Packed Towers: Type of Packing: NA Superficial Gas Velocity through Bed:

Gas Stream Characteristics

21. Gas flow into the collector: 1000 ACF @ 20 °F and 14.2 PSIA	22. Gas stream temperature: Inlet: ambient °F Outlet: ambient °F
23. Gas flow rate: Design Maximum: 135 ACFM Average Expected: 67 ACFM	24. Particulate Grain Loading in grains/scf: Inlet: NA Outlet: NA

25. Emission rate of each pollutant (specify) into and out of collector:					
Pollutant	IN		OUT		Guaranteed Minimum Collection Efficiency
	lb/hr	grains/acf	lb/hr	grains/acf	
A HCl	0.03lb/hr		0.0003lb/hr		99
B					
C					
D					
E					

26. Type of pollutant(s) controlled: <input type="checkbox"/> SO _x <input type="checkbox"/> Odor <input type="checkbox"/> Particulate (type): <input checked="" type="checkbox"/> Other: HCl
27. By what method were the uncontrolled emissions calculated? <input checked="" type="checkbox"/> Material Balance <input type="checkbox"/> Stack Test <input type="checkbox"/> Pilot Test <input type="checkbox"/> Other:
28. Dimensions of stack: Height 4'-9" ft. Diameter 5'-1" ft
29. Supply an equilibrium curve and/or solubility data (at various temperatures) for the proposed system.
30. Supply a curve showing proposed collection efficiency versus gas volume from 25 to 100 percent of design rating of collector.

Particulate Distribution

31. Complete the table:		
Particulate Size Range (microns)	Particle Size Distribution at Inlet to Collector	Fraction Efficiency of Collector
	Weight % for Size Range	Weight % for Size Range
0 – 2	NA, vapor to liquid solvent conversion.	
2 – 4		
4 – 6		
6 – 8		
8 – 10		
10 – 12		
12 – 16		
16 – 20		
20 – 30		
30 – 40		
40 – 50		
50 – 60		
60 – 70		
70 – 80		
80 – 90		
90 – 100		
>100		
32. Describe any air pollution control device inlet and outlet gas conditioning processes (e.g., gas cooling, gas reheating, gas humidification):		
33. Describe the collection material disposal system: Neutralized HCl gas will become a salt brine that will be disposed of in accordance with local, state (PADEP), and federal regulations.		
34. Have you included Wet Collecting (Scrubber) Control Device in the Emissions Points Data Summary Sheet? Yes		

35. Proposed Monitoring, Recordkeeping, Reporting, and Testing Please propose monitoring, recordkeeping, and reporting in order to demonstrate compliance with the proposed operating parameters. Please propose testing in order to demonstrate compliance with the proposed emissions limits.	
MONITORING:	RECORDKEEPING:
REPORTING:	TESTING:
MONITORING: Please list and describe the process parameters and ranges that are proposed to be monitored in order to demonstrate compliance with the operation of this process equipment or air control device. RECORDKEEPING: Please describe the proposed recordkeeping that will accompany the monitoring. REPORTING: Please describe any proposed emissions testing for this process equipment on air pollution control device. TESTING: Please describe any proposed emissions testing for this process equipment on air pollution control device.	
36. Manufacturer's Guaranteed Capture Efficiency for each air pollutant.	
37. Manufacturer's Guaranteed Control Efficiency for each air pollutant. 0.99%	
38. Describe all operating ranges and maintenance procedures required by Manufacturer to maintain warranty.	

**Attachment L
EMISSIONS UNIT DATA SHEET
BULK LIQUID TRANSFER OPERATIONS**

Furnish the following information for each new or modified bulk liquid transfer area or loading rack, as shown on the *Equipment List Form* and other parts of this application. This form is to be used for bulk liquid transfer operations such as to and from drums, marine vessels, rail tank cars, and tank trucks.

Identification Number (as assigned on <i>Equipment List Form</i>):				
1. Loading Area Name:				
2. Type of cargo vessels accommodated at this rack or transfer point (check as many as apply): <input type="checkbox"/> Drums <input type="checkbox"/> Marine Vessels <input type="checkbox"/> Rail Tank Cars <input checked="" type="checkbox"/> Tank Trucks				
3. Loading Rack or Transfer Point Data:				
Number of pumps				
Number of liquids loaded	2			
Maximum number of marine vessels, tank trucks, tank cars, and/or drums loading at one time	1			
4. Does ballasting of marine vessels occur at this loading area? <input type="checkbox"/> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> Does not apply				
5. Describe cleaning location, compounds and procedure for cargo vessels using this transfer point:				
6. Are cargo vessels pressure tested for leaks at this or any other location? <input type="checkbox"/> Yes <input type="checkbox"/> No If YES, describe:				
7. Projected Maximum Operating Schedule (for rack or transfer point as a whole):				
Maximum	Jan. - Mar.	Apr. - June	July - Sept.	Oct. - Dec.
hours/day				
days/week				

TM = Test Measurement based upon test data submittal
O = other (describe)

9. Proposed Monitoring, Recordkeeping, Reporting, and Testing

Please propose monitoring, recordkeeping, and reporting in order to demonstrate compliance with the proposed operating parameters. Please propose testing in order to demonstrate compliance with the proposed emissions limits.

MONITORING	RECORDKEEPING
REPORTING	TESTING

MONITORING. PLEASE LIST AND DESCRIBE THE PROCESS PARAMETERS AND RANGES THAT ARE PROPOSED TO BE MONITORED IN ORDER TO DEMONSTRATE COMPLIANCE WITH THE OPERATION OF THIS PROCESS EQUIPMENT OPERATION/AIR POLLUTION CONTROL DEVICE.

RECORDKEEPING. PLEASE DESCRIBE THE PROPOSED RECORDKEEPING THAT WILL ACCOMPANY THE MONITORING.

REPORTING. PLEASE DESCRIBE THE PROPOSED FREQUENCY OF REPORTING OF THE RECORDKEEPING.

TESTING. PLEASE DESCRIBE ANY PROPOSED EMISSIONS TESTING FOR THIS PROCESS EQUIPMENT/AIR POLLUTION CONTROL DEVICE.

10. Describe all operating ranges and maintenance procedures required by Manufacturer to maintain warranty

--



101 FAIRVIEW AVENUE
PITTSBURGH, PA 15238

EMAIL: SALES@V-SYST.COM
WEB: WWW.V-SYST.COM

TELEPHONE: 412-826-9200
FAX: 412-826-8168

Quote #2023-560-H-R

July 26, 2023

Mr. Farley R. Wood, P.E.
Vice President of Engineering
Empire Diversified Energy
1400 Main Street
Follansbee, WV 26037

Subject: Chemical System - Scrubber -- Quote #2023-560-H-R

Dear Mr. Wood,

Please find attached our proposal for the above referenced equipment/project. We appreciate the opportunity to provide a quote for this opportunity.

You will also find our most recent line card attached for your reference. I hope you will think of us during your next project. If you would have any questions or require additional information, please give us a call at (412) 826-9200.

Sincerely,

Russell C. Huffmyer
President & CEO
V-Systems, Inc.
101 Fairview Avenue
Pittsburgh, PA 15238

Enclosure

arsr

TOLL FREE: 1 (888) 826-0225



EMAIL: SALES@V-SYST.COM

* V-SYSTEMS, YOUR ONE STOP FOR YOUR INDUSTRIAL & COMMERCIAL HVAC, PLUMBING AND FIRE PROTECTION SUPPLIES *



101 FAIRVIEW AVENUE
PITTSBURGH, PA 15238

EMAIL: SALES@V-SYST.COM
WEB: WWW.V-SYST.COM

TELEPHONE: 412-826-9200
FAX: 412-826-8168

Quotation:

Project Name: Chemical System - Scrubber **Contact Name:** Farley Wood
Company Name: Empire Diversified Energy **Email/Fax:** fwood@empirede.com
Address/Street: 1400 Main Street **Phone:** 304-914-2624
City/State/Zip: Follansbee, WV 26037 **Date:** July 21, 2023 / Revised July 26, 2023
Quote Number: 2023-560-H-R

Thank you for the opportunity to provide you with the following quote:

Quantity	Item Description	Net Price Each	Total Net Price
Tag: Scrubber Tank			
1	PolyScrub Scrubber Tank, 700 Open Top, Rated: 1.90 Specific Gravity Wall Thickness, Material: Crosslinked Polyethylene (XLPE)♦, Color: Natural (yellowish white) <ul style="list-style-type: none"> • (1) Lid/Manway - 61" Cover Assembly Open Top /Stainless Steel/Pe • (1) Vent - 6" U-Vent PVC • (1) Outlet / Overflow - 1" Scrubber Outlet/Overflow PVC/litharge Viton /c-276 • (1) Scrubber - 6" Scrubber Assembly PVC/litharge Viton • (1) Fill - 1" Bulkhead Fitting Assembly Socket x thread PVC/litharge Viton • Warranty - 5 Years, Full Replacement, Non-Prorated Includes Product Engineering / Permitting Support for Permit Application	\$16,500.00	\$16,500.00
Tag: Tank			
1	10,305-Gallon Vertical Tank, Rated: 1.90 Specific Gravity Wall Thickness, Material: Crosslinked Polyethylene (XLPE)♦, Color: Natural (yellowish white) <ul style="list-style-type: none"> • (1) Lid/Manway - 24" Manway Cover 24" Fume Tight /Stainless Steel/pe • (1) Fill - 2" Bulkhead Fitting Assembly Socket x thread PVC/EPDM • (2) Dome Fitting - 2" Bulkhead Fitting Assembly Socket x thread PVC/EPDM • (3) Sidewall Fitting - 2" Bolted Flange Fitting Socket PVC/c-276/EPDM • (1) Vent - 6" U-vent with Bolted Flange PVC/c-276/EPDM • WARRANTY:5 Years, Full Replacement, Non-Prorated 	\$39,675.00	\$39,675.00

V-SYSTEMS

COMMERCIAL | INDUSTRIAL | MUNICIPAL

101 FAIRVIEW AVENUE
PITTSBURGH, PA 15238

EMAIL: SALES@V-SYST.COM
WEB: WWW.V-SYST.COM

TELEPHONE: 412-826-9200
FAX: 412-826-8168

Tag: Pump

2	March Model # TE-10K-MD 3PH 10 HP - Inlet: 3"MPT, Outlet: 2"MPT, Wet End: Natural Kynar (Front Housing, Rear Housing), Glass Filled Kynar (Impeller) with 6.625" Impeller Trim, Viton (Gasket), Carbon (Bushing), Ceramic (Shaft, Thrust Washers), and driven by a 10 HP, 3500 RPM, 3/60/230/460, TEFC Motor	\$7,920.00	\$15,840.00
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Note:

- Lead Time is currently 1 Week, A.R.O.
- FOB out of March in IL (must ship by LTL due to size and weight)

Tag: VFD(s)

2	Xylem, Variable Frequency Drives, 10 HP, 460-3-60, NEMA 3R, BACnet	\$7,780.00	\$15,560.00
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Note:

- Lead Time is currently at 7 Weeks, A.R.O.

Tag: Chem Feed Skid

1	SS1-C_FLOOR_050_PVCEPDM_PD PP/PE Prominent Skid for solenoid driven pumps, (20"W x 18"D x 40"H) 1/2" PVC/EPDM socket weld pipe and fittings Wye strainer 500ml PVC calibration column 164ml CPVC/EPDM pulsation dampeners Pressure relief valves Pressure gauge with isolator Back pressure valve Plumbing and components rated at 150 PSI regardless of pump pressure.	\$21,505.00	\$21,505.00
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- (1) GMXA0708PVT2Q000UDC1300EN Prominent Gamma/X 2 GPH/102PSI, PVDF/PTFE, bleed valve w/spring, 4-20mA output
- (1) Prominent CP1 ONE PUMP 120VAC SCADA PANEL

Total Quoted Amount: \$109,080.00

QUOTED BY: RUSS HUFFMYER

If you need further information concerning the products that have been included in the quote, please feel free to contact me at 412-826-9200 and/or rhuffmyer@v-syst.com.

We appreciate the opportunity to provide you with this quote and look forward to working with you on this important project.

Thank you,



Russell C. Huffmyer
President & CEO

arsr



101 FAIRVIEW AVENUE
PITTSBURGH, PA 15238

EMAIL: SALES@V-SYST.COM
WEB: WWW.V-SYST.COM

TELEPHONE: 412-826-9200
FAX: 412-826-8168

THIS QUOTATION OR SELLER'S ACCEPTANCE OF THIS ORDER IS EXPRESSLY LIMITED TO, AND EXPRESSLY MADE CONDITIONAL ON, BUYER'S ACCEPTANCE OF THE V-SYSTEMS-TEC, INC. STANDARD TERMS AND CONDITIONS OF SALE. A COPY OF THESE TERMS AND CONDITIONS IS AVAILABLE AT <https://v-syst.com/terms-and-conditions-of-sale-and-service>. SELLER OBJECTS TO ANY DIFFERENT OR ADDITIONAL TERMS.

General Comments

Warranty applies per Sales & Service Terms and Conditions if the following are met:

- Equipment installed per industry standards and manufacturer instruction manual.
- Operation of equipment in accordance with manufacturer instruction manual.
- Maintenance and lubrication per manufacturer instruction manual. Note, maintenance log showing dates required.
- Equipment must be stored per manufacturer instruction manual and protected from the weather.

If warranty items occur, V-Systems needs to be contacted in writing before any repairs are made, whereas a mutual course of action will be performed. Equipment cannot be disassembled without V-Systems being present.

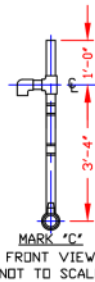
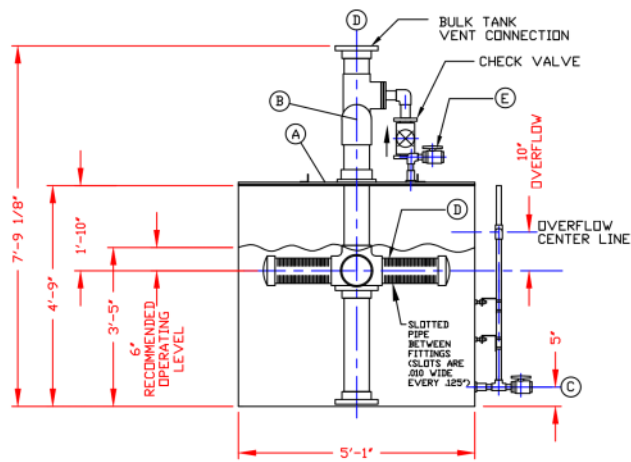
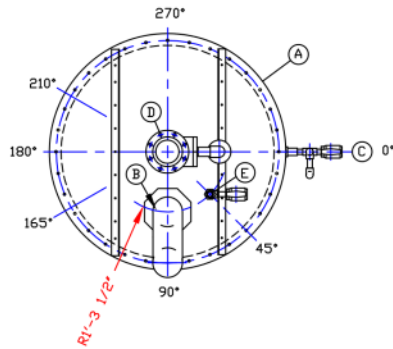
Acknowledged and Accepted by Buyer:

Name: _____ *Tax Exempt? Yes ___ No ___

Signature: _____ PO #: _____


Date: _____ Ship To: _____

*IF APPLICABLE, please send a copy of your company's tax-exempt form. Otherwise, our accounting department will assume that this order is taxable.

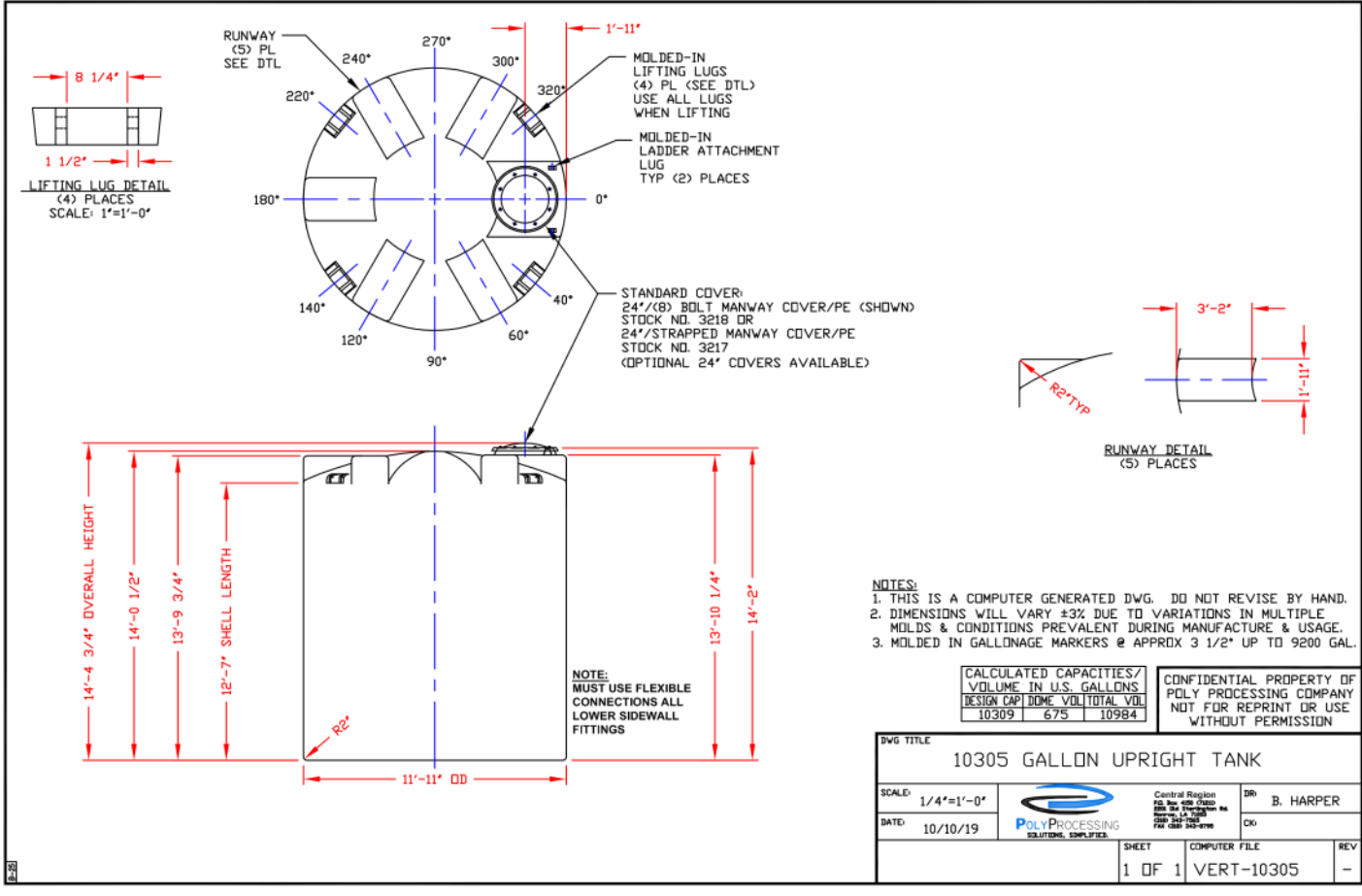


NOTE: INCOMING VENT PIPE MUST BE INDEPENDENTLY SUPPORTED ELEVATIONS ONLY-- NOZZLES & ACCESSORIES ROTATED INTO VIEW-- FOR TRUE ORIENTATION SEE PLAN VIEW

- NOTES**
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 2. DIMENSIONS WILL VARY ±3% DUE TO VARIATIONS IN MULTIPLE MOLDS & CONDITIONS PREVALENT DURING MANUFACTURE & USAGE.
 3. TANK DESIGNED FOR 1.9 SpG MAT'L @ 100°F/ATMOS PRESSURE.

DWG TITLE		POLYSCRUB BASIC	
		5' X 5' SCRUBBER	
SERVICE: SCRUBBER MEDIA		1.9 SpG/XLPE/NATURAL	
SCALE:	1/2"=1'-0"		DR: B. HARPER
DATE:	4/12/2021		CR:
CALCULATED CAPACITY TO OPERATING LEVEL		SHEET	COMPUTER FILE
-515 GALLONS		1 OF 1	POLYSCRUB BASIC


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 3. MOLDED IN GALLONAGE MARKERS @ APPROX 3 1/2" UP TO 9200 GAL.

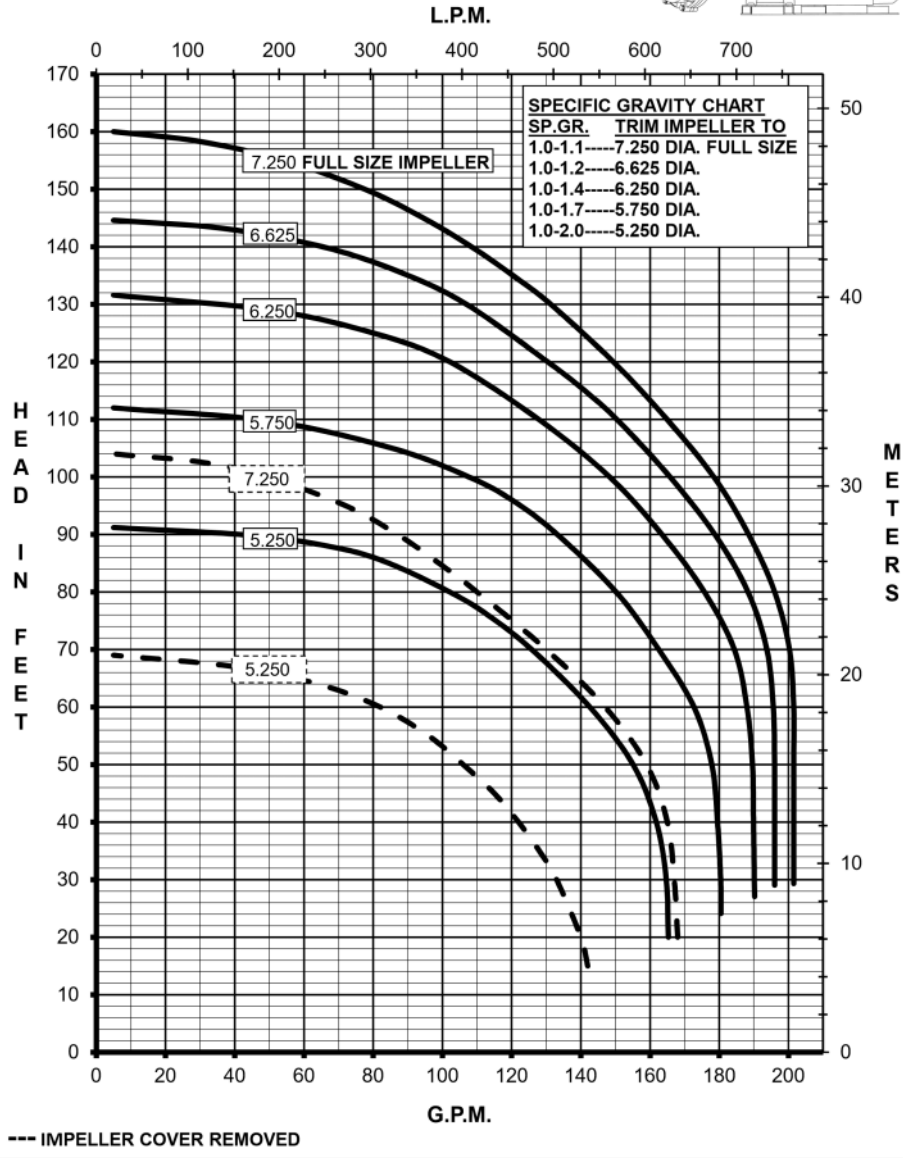
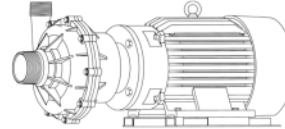
CALCULATED CAPACITIES/ VOLUME IN U.S. GALLONS		
DESIGN CAP	DOME VOL	TOTAL VOL
10309	675	10984

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DWG TITLE			
10305 GALLON UPRIGHT TANK			
SCALE:	1/4"=1'-0"	 Central Region 200 New 40th Street Pittsboro, NC 27566 919.541.1100 FAX 919.541.1199	DR:
DATE:	10/10/19		CK:
SHEET		COMPUTER FILE	REV
1 OF 1		VERT-10305	-

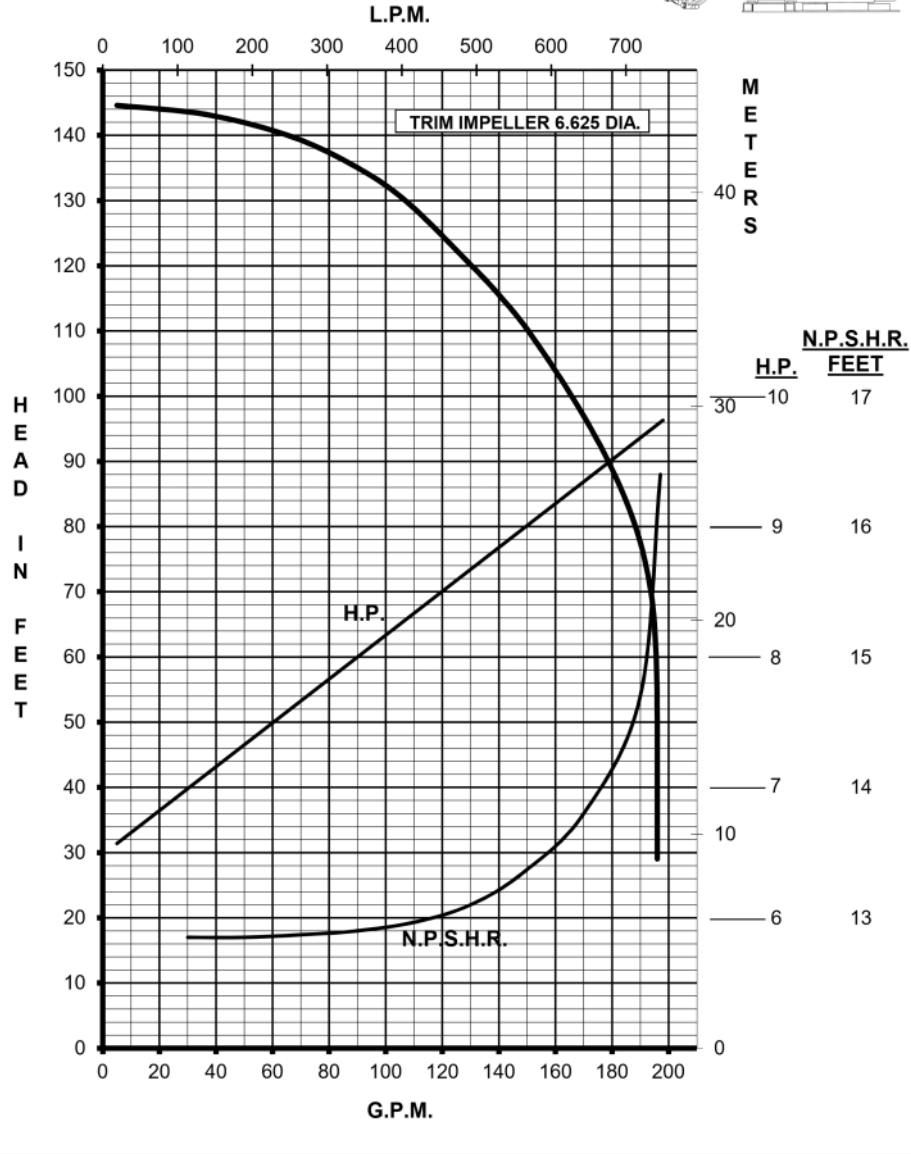
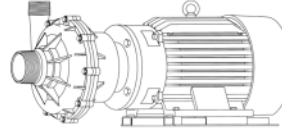


TE-10K-MD, TE-10P-MD
3PH 60HZ TRIM CURVES





MARCH TE-10K-MD, TE-10P-MD
PUMPS TRIM IMPELLER 6.625 DIA.
 3PH 60HZ



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- Firetube Design
- Natural Gas, Propane, #2 Fuel Oil, True Dual Fuel (NG & #2 Oil)
- Size Range: 4 to 2500 HP

Hydronic Boilers

- Efficiencies up to 99.1%
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- Natural Gas, Propane, #2 Fuel Oil, True Dual Fuel (MG & #2 Oil)
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Additional Offerings:

- Thermal Fluid Heaters
- Ancillary Equipment
- Custom Engineered Systems



Hydronic Boilers

- Models from 55,000 to 6.0 Million Btu/Hr
- Up to 96.2% Thermal Efficiency
- Up to 25:1 Turndown Ratio
- Featuring CON-X-US® Remote Connectivity and SMART TOUCH™ Operating Control

Thermal Fluid Heaters

- Models from 125,000 to 4,000,000 Btu/Hr
- Up to 99% Thermal Efficiency
- Up to 10:1 Turndown Ratio
- Direct Vent Flexibility up to 150 Ft.
- SMART TOUCH™ Operating Control and CON-X-US® Remote Connect

Additional Offerings:

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- Base Mounted
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- Electric & Diesel Driven Systems
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Performance Range:

- Up to 28,000 US GPM flow
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Temperature:

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Contact:

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- 412-826-9200

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Products: Thermostatic Mixing Valves
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Carter Pump	Pumps 2000
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Xylem / G & L Pumps	Stancor / Flow Solutions
Hydroflo Pumps (Taco Group)	Tigerflow

BOILERS & WATER HEATERS

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Baldor Motors (ABB)	SEE Water Controls
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Flomatic Valves	Sure Flow Company
Holby Valve Co.	Titan Flow Control
Macon Controls	

GAUGES

Terrice	Weiss Instruments
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HYDRONICS

Gerand Engineering	Tunstall
Pro Hydronic Specialties	

FIRE PROTECTION

Armstrong	Tornatech
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PIPING

Energy Task Force (Underground Piping Solutions)

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Aqua Turbo Systems	EcoVerde
Active Water Solutions	Equip Water
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2401 Parkman Road NW
Warren, OH 44485

(330) 394-4747, Ext. 1502

About Us	Facilities & Equipment	Bottom Line
<p>Warren Design & Build is a multi-disciplined machine shop and engineering design services company. We specialize in emergency repairs of part and machines, as well as building custom machines.</p> <p>Our team is comprised of 10 machinists, 4 welders, 4 mechanical and electrical design engineers with in-house PLC and computer systems programming capability.</p>	<p>Located in Warren Ohio, WDB's 38,000 square foot corporate facility houses a variety of engineering, machining, assembly, and fabricating capabilities. Our large assembly area can handle everything from a single station to a full assembly line with all utilities available utilizing ceiling drops from electrical bus bar and pneumatic lines covering most of the floor space.</p> <p>Located in the Northeast Ohio Manufacturing Corridor we also have the availability to outsource many special processes that can be brought onboard on short notice to assist in peak design periods or on special projects.</p>	<p>With WDB's unique position of having all Design, Machining, Paint, Mechanical and Electrical Assembly under one roof, our engineering team has the ability to assist in all aspects of the program build cycle to ensure design integrity; and when necessary, capture all changes and updates as required by manufacturing, and/or requested by the customer, in a very economical time frame.</p> <p>With some of Northeast Ohio's most talented, experienced, and highly trained engineering and manufacturing staff we can help guide you with suggestions and input that will help maximize your project's efficiency, while often lowering costs.</p>



201 Chambers Street
McKees Rocks, PA 15136

(412) 771-5160

About Us	Facilities & Equipment	Bottom Line
<p>AJ Drgon, a subsidiary of Custom Machine and Design is a multi-disciplined machine shop and engineering design services company. We specialize in emergency machining services and repairs of parts and machines, as well as building custom machines.</p> <p>Our team is comprised of 4 machinists, 1 welder and 1 mechanical design engineer. Additionally, we partner with our sister company, Warren Design & Build for many other services.</p>	<p>Located in McKees Rocks PA, AJ Drgon's 8,000 square foot facility houses a variety of engineering, machining, assembly, and fabricating capabilities.</p> <p>Located near downtown Pittsburgh, we also have the availability to outsource many special processes that can be brought onboard on short notice to assist in peak design periods or on special projects.</p>	<p>With AJ Drgon's unique position of having all Design, Machining, Paint, Mechanical and Electrical Assembly under one roof, our engineering team has the ability to assist in all aspects of the program build cycle to ensure design integrity; and when necessary, capture all changes and updates as required by manufacturing, and/or requested by the customer, in a very economical time frame.</p> <p>With some of Pittsburgh's most talented, experienced, and highly trained engineering and machining staff we can help guide you with suggestions and input that will help maximize your project's efficiency, while often lowering costs.</p>



Capabilities



- Emergency Repair: We fix all electro-mechanical devices. We have field tech service and in-house staff that will repair all forms of equipment.
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We can support your engineering with control programming support.



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NHSM Response to RIR 3/7/2024

Wednesday, March 27, 2024 2:03 PM



Andrews, Edward S <edward.s.andrews@wv.gov>

RE: Regulatory Interpretation Request - EGG

2 messages

Morrison, Jacqueline <Morrison.Jacqueline@epa.gov>
To: "edward.s.andrews@wv.gov" <edward.s.andrews@wv.gov>
Cc: "Supplee, Gwendolyn" <Supplee.Gwendolyn@epa.gov>

Thu, Mar 7, 2024 at 3:32 PM

Hi Ed,

Thanks for sending. We will get back to you, but I'd assume that the response from the waste perspective will be similar to when we last considered this facility last year.

Thank you.

Jacque

Jacqueline Morrison

RCRA Programs Section, Hazardous Waste
Land, Chemicals, & Redevelopment Division
Mail Code 3LD31

US EPA Mid-Atlantic Region

Address: Four Penn Center,
1600 John F. Kennedy Boulevard,
Philadelphia, PA 19103-2852

Phone: 215-814-5664

Email: morrison.jacqueline@epa.gov

From: Andrews, Edward S <edward.s.andrews@wv.gov>
Sent: Wednesday, March 06, 2024 3:35 PM
To: Willson, Matthew (he/him/his) <Willson.Matthew@epa.gov>; Morrison, Jacqueline <Morrison.Jacqueline@epa.gov>
Subject: Fwd: Regulatory Interpretation Request - EGG

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FYI on a Regulatory Interpretation Request

Thanks,

Ed

----- Forwarded message -----

From: **Andrews, Edward S** <edward.s.andrews@wv.gov>

Date: Wed, Mar 6, 2024 at 2:54 PM

Subject: Regulatory Interpretation Request - EGG

To: Cristina Fernandez <fernandez.cristina@epa.gov>, Supplee, Gwendolyn <supplee.gwendolyn@epa.gov>, Marycate Opila <opila.marycate@epa.gov>

Cc: Beverly D Mckeone <beverly.d.mckeone@wv.gov>, Crowder, Laura M <laura.m.crowder@wv.gov>

Please see the attached file (Reg_Inter_Req_for_EGG) from the WVDEP/DAQ Regulatory Interpretation Request regarding Empire Green Generation's proposed pyrolysis units processing plastic feedstock.

Should you or your staff have any questions about this request, please let me know.

Thanks,

Ed

--

Edward Andrews, P.E.

Engineer

WVDEP/Division of Air Quality

304-926-0499 Ext 41244

[601 57th Street, SE](#)

[Charleston, WV 25304](#)

--

Edward Andrews, P.E.

Engineer

WVDEP/Division of Air Quality

304-926-0499 Ext 41244

601 57th Street, SE

Charleston, WV 25304

Andrews, Edward S <edward.s.andrews@wv.gov>

Fri, Mar 8, 2024 at 7:38 AM

Draft To: "Morrison, Jacqueline" <Morrison.Jacqueline@epa.gov>

Cc: "Supplee, Gwendolyn" <supplee.gwendolyn@epa.gov>, Krystal <Stankunas.Krystal@epa.gov>

Please keep in mind that the facility has elected to change from processing medical waste to plastic feedstock. I have been trying to get them to perform a waste/non-waste determination of this plastic feedstock in accordance with Part 241.

EGG keeps pushing back with a State House bill that defined "advance recycling" and "high temperature under WV

[Quoted text hidden]

Follow-up on Timing for the RIR 3/7/2024

Wednesday, March 27, 2024 2:02 PM



Andrews, Edward S <edward.s.andrews@wv.gov>

Re: Regulatory Interpretation Request - EGG

1 message

Andrews, Edward S <edward.s.andrews@wv.gov>

Thu, Mar 7, 2024 at 2:32 PM

To: "Supplee, Gwendolyn" <Supplee.Gwendolyn@epa.gov>

Cc: Beverly D Mckeone <beverly.d.mckeone@wv.gov>, "Stankunas, Krystal" <Stankunas.Krystal@epa.gov>

Gwen,

We understand that this is fairly complicated and that we expected multiple different offices to be called on to provide input to our request.

Please keep in mind that EGG has a permit to process medical waste using the same equipment. The other real changes to the process is adding the HCI tanks and loadout station.

So, EGG will be applying pressure at some point to get their application moving forward in the near future.

We expect to send EGG an additional information request based on your office's response.

At some point, we will have to move this application forward to some sort of decision with or without a response.

Please provide us some sort of response by no later than March 29.

Thanks,
Ed

On Thu, Mar 7, 2024 at 1:11 PM Supplee, Gwendolyn <Supplee.Gwendolyn@epa.gov> wrote:

Hi Ed,

We need to coordinate with our RCRA program as well as potentially Headquarters (either for RCRA or CAA requirements) and that coordination can take some time. Since the application hasn't been deemed complete yet, would it be OK if we try to get a response to West Virginia by the end of March? We'll try to get a response sooner if we can.

Many thanks.

-gwen



Air & Radiation Division

Phone 215-814-2763

Email supplee.gwendolyn@epa.gov

From: Andrews, Edward S <edward.s.andrews@wv.gov>
Sent: Thursday, March 07, 2024 10:54 AM
To: Supplee, Gwendolyn <Supplee.Gwendolyn@epa.gov>
Cc: Beverly D Mckeone <beverly.d.mckeone@wv.gov>; Stankunas, Krystal <Stankunas.Krystal@epa.gov>
Subject: Re: Regulatory Interpretation Request - EGG

Caution: This email originated from outside EPA, please exercise additional caution when deciding whether to open attachments or click on provided links.

Gwendolyn,

WVDEP/DAQ received the initial application on December 1, 2023, and a revised application was received January 23, 2024. Currently, this application has not been deemed complete at this time.

Therefore, the regulatory clock has not started yet.

We would like some sort of response from your office within 2 weeks. A response to our request will dictate our future request for additional information from this applicant (EGG).

Should you have any questions about this, please do not hesitate to contact me.

Thanks

Ed

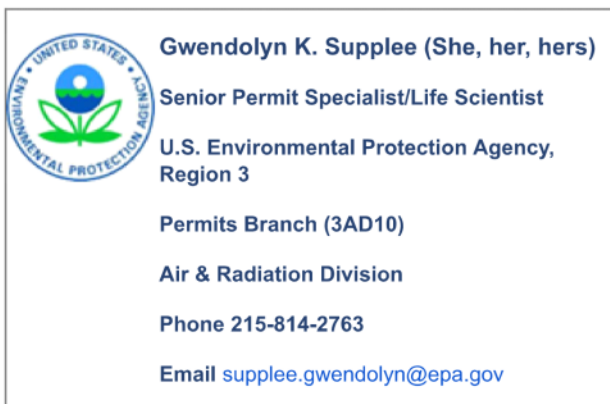
On Thu, Mar 7, 2024 at 10:30 AM Supplee, Gwendolyn <Supplee.Gwendolyn@epa.gov> wrote:

Ed-

Can you tell us when the application was received and what date the permitting decision must be made by? In looking at WV's R13 rule, it looks like a permit must be issued within 90 days of the completeness determination? Is my interpretation correct? We're trying to determine when WV needs a response by.

Many thanks,

-gwen



From: Andrews, Edward S <edward.s.andrews@wv.gov>

Sent: Wednesday, March 06, 2024 2:55 PM

To: Fernandez, Cristina <Fernandez.Cristina@epa.gov>; Supplee, Gwendolyn <Supplee.Gwendolyn@epa.gov>;
Opila, MaryCate <Opila.MaryCate@epa.gov>

Cc: Beverly D Mckeone <beverly.d.mckeone@wv.gov>; Crowder, Laura M <laura.m.crowder@wv.gov>

Subject: Regulatory Interpretation Request - EGG

Caution: This email originated from outside EPA, please exercise additional caution when deciding whether to open attachments or click on provided links.

Please see the attached file (Reg_Inter_Req_for_EGG) from the WVDEP/DAQ Regulatory Interpretation Request regarding Empire Green Generation's proposed pyrolysis units processing plastic feedstock.

Should you or your staff have any questions about this request, please let me know.

Thanks,

Ed

--

Edward Andrews, P.E.

Engineer

WVDEP/Division of Air Quality

304-926-0499 Ext 41244

601 57th Street, SE

Charleston, WV 25304

--

Edward Andrews, P.E.

Engineer

WVDEP/Division of Air Quality

304-926-0499 Ext 41244

601 57th Street, SE

Charleston, WV 25304

Regulatory Interpretation Request 3/6/2024

Wednesday, March 27, 2024 2:00 PM



Andrews, Edward S <edward.s.andrews@wv.gov>

Regulatory Interpretation Request - EGG

1 message

Andrews, Edward S <edward.s.andrews@wv.gov>

Wed, Mar 6, 2024 at 2:54 PM

To: Cristina Fernandez <fernandez.cristina@epa.gov>, "Supplee, Gwendolyn" <supplee.gwendolyn@epa.gov>, Marycate Opila <opila.marycate@epa.gov>

Cc: Beverly D Mckeone <beverly.d.mckeone@wv.gov>, "Crowder, Laura M" <laura.m.crowder@wv.gov>

Bcc: Brian S Tephacock <Brian.S.Tephacock@wv.gov>, Eric Blend <eric.n.blend@wv.gov>

Please see the attached file (Reg_Inter_Req_for_EGG) from the WVDEP/DAQ Regulatory Interpretation Request regarding Empire Green Generation's proposed pyrolysis units processing plastic feedstock.


Should you or your staff have any questions about this request, please let me know.

Thanks,
Ed

--

Edward Andrews, P.E.
Engineer
WVDEP/Division of Air Quality
304-926-0499 Ext 41244
601 57th Street, SE
Charleston, WV 25304

2 attachments

 **R13-3555 Modification_Application_EGG - Redacted_Final Rev.pdf**

22432K

 **Reg_Interp_Request_for_EGG.pdf**

400K



Reg_Interp
_Request...



west virginia department of environmental protection

Division of Air Quality
601 57th Street, SE
Charleston, WV 25304
(304) 926-0475

Harold D. Ward, Cabinet Secretary
dep.wv.gov

March 6, 2023

Ms. Christina Fernandez
Director
U.S. EPA - Region 3
Air and Radiation Division
Four Penn Center
1600 John F. Kennedy Boulevard
Philadelphia, PA 19103-2852

Re: Regulatory Interpretation Request
Empire Green Generation LLC
Facility ID: 009-00141
Permit No.: R13-3555A
Follansee, WV

Dear Director:

The West Virginia Department of Environmental Protection - Division of Air Quality (DAQ) respectfully requests an regulatory interpretation from the Administrator regarding Empire Green Generation's (EGG) proposed modification of their Follansee, West Virginia Facility to any regulation developed under Section 129 of the Clean Air Act.

Specifically, the DAQ is requesting an regulatory interpretation as to whether all streams, or only the liquid and solid streams, exiting the pyrolysis process need to be evaluated under 40 CFR 241 to determine applicability under 40 CFR 60, Subpart CCCC, if the plastic feedstock to the pyrolysis process has been determined to be a fuel or raw material under 40 CFR 241.

The DAQ does not believe that EGG pyrolysis trains or downstream emission units (e.g., engines, dryer, and vitrifier) would be affected sources under Subpart AAAA and EEEE because the plastic feedstock does not meet the definition of municipal solid waste and the Follansee Facility is not an institutional facility.

Promoting a healthy environment.

Background Information

In 2022, Empire Green Generation LLC (EGG) proposed to the DAQ to construct and operate two pyrolysis trains with gas cleaning sections to process and convert up to 70 tons per day of medical waste into tar (liquids), char (solids) and synthetic gas.

The DAQ issued Permit R13-3555 to EGG on March 2, 2023. During the DAQ review of the Application, the DAQ determined that EGG's proposed pyrolysis trains meet the criteria of a "pyrolysis unit" as defined in 40 CFR 60.51c and therefore the proposed pyrolysis trains are excluded emission units from Subpart Ec.

Proposed Modification

On December 1, 2023, EGG filed a modification application with the DAQ. EGG proposed to replace the medical waste feedstock with plastic feedstock. In a revised application (January 23, 2024, Submission), EGG noted that the feedstock will be sourced from recyclers, manufacturing, and plastic producers. This pre-processed plastic feedstock will be shipped to EGG's Follansbee, WV facility as feedstock for the pyrolysis trains.

EGG noted that this modification only requires the addition of a hydrochloric acid truck loading facility with associated scrubber system. This feedstock change will allow the pyrolysis trains to generate hydrochloric acid in addition to other products (tars, char, and synthetic gas).

The processing capacity of these pyrolysis trains will remain the same at 35 tons of plastic feedstock per day per pyrolysis train (70 Tons per day total).

Regulatory Considerations

EGG commenced construction of the pyrolysis trains in 2023, which is after the applicability date of Subparts AAAA (August 30, 1999); CCCC (June 4, 2010); and EEEE (December 9, 2004). Therefore, EGG's pyrolysis trains meet the definition of new affected units.

Given the design capacity of the two pyrolysis trains, these units do not meet the capacity criteria of a large municipal waste combustion unit as defined under Subpart Eb and therefore, the units are not subject to Subpart Ec.

The DAQ determined that the four spark ignition engines are affected sources with regard to Subpart JJJJ during the review of Permit R13-3555. However, the DAQ was unable to determine the applicable emission standard to which the permit engines were subject. Condition 5.1.1. of Permit R13-3555 required EGG to seek a determination from the EPA to determine which emission standard would be applicable for these four engines.

The vitrifiers (process heaters) for the pyrolysis trains may be affected sources under Subpart Dc of Part 60 and Subpart JJJJJ of Part 63. Applicability status for these process heaters would be affected by the outcome of this determination. These units are designed to fire gaseous fuel (synthetic gas), liquid fuel (tars), propane for startup operations only, or a combination of synthetic gas and tars with a maximum heat input of 100 MMBtu/hr.

Past Determinations and Other Permitting Actions

Prior to submitting this determination, the DAQ searched the Applicability Determination Index (ADI) for similar determinations, and identified the following:

Table 1 - Similar Applicability Determinations			
EPA Office	Control Number	Date	Reference
Region 5	9700062	10/11/1996	60.14, 60.15, 60.5, 60.51b,
Region 6	NR06	02/07/1985	52.21(b), 60.50, 60.51(b)
Region 7	9600096	12/02/1996	60.50b
Region 10	E010	04/12/1977	60.50, 60.51
DSSE	E009	01/19/1977	60.50
Region 1	M140002	12/04/2012	40 CFR 60, Subpart EEEE
Region 9	1000019	03/30/2010	40 CFR 60, Subpart AAAA
Region 10	1500025	08/31/2010	40 CFR 60, Subpart AAAA
Region 4	1700010	03/02/2017	40 CFR 60, Subpart CCCC
Region 5	1800003	01/22/2018	40 CFR 60, Subpart CCCC

The DAQ is aware of several determinations by other State Agencies, listed below:

Table 2 - List of Similar State Actions				
State Agency	Company/Permittee Name	Permit No.	Date	Outcome
Indiana Department of Environmental Management	Fulcrum Centerpoint LLC	089-44042-00660	08/16/2022	Meet exemption under 60.1020(h)
North Carolina Environmental Quality	Braven Environmental LLC	10672R00	9/25/2020	No Reference
Indiana Department of Environmental Management	Brightmark Plastics Renewal Indiana 2 LLC	151-45294-00067	06/29/2022	Meet exemption under 60.1020(h)
Ohio Environmental Protection Agency	SOBE Thermal Energy Systems, LLC	P0132799	02/14/2024	Scrap Tires are classified as non-waste per 40CFR241. Not Applicable to any incinerator rules

The DAQ is aware of EPA's decision to not remove the phrase "pyrolysis/combustion unit" for the definition of *municipal waste combustion unit* in Subparts AAAA and EEEE of Part 60.¹

The DAQ is working under the assumption that EGG's plastic feedstock is non-hazardous per 40 CFR 262.

First Question: *Should EGG's plastic feedstock be viewed as waste or non-waste?*

The DAQ believes that the proper way to answer this question is for EGG/EGG's plastic feedstock provider to make a waste/non-waste determination of this plastic feedstock in accordance with 40 CFR 241. Based on EGG's application and additional responses regarding this question, EGG may have determined or believe that the plastic feedstock is a non-waste. EGG has not provided any information that DAQ would view as an official determination in accordance with 40 CFR 241.

¹ Standards of Performance for New Stationary Sources and Emission Guidelines for Existing Sources: Other Solid Waste Incineration Units Review; Withdrawal of Proposed Provision Removing Pyrolysis/Combustion Units, 88 Fed. Reg. 36524 (June 5, 2023).

DAQ looked at the definitions that pertain to waste under potentially applicable subparts, which are as follows:

“Solid waste” is defined under Subpart EEEE as

“means any garbage, refuse, sludge from a waste treatment plant, water supply treatment plant, or air pollution control facility and other discarded material, including solid, liquid, semisolid, or contained gaseous material resulting from industrial, commercial, mining, agricultural operations, and from community activities, but does not include solid or dissolved material in domestic sewage, or solid or dissolved materials in irrigation return flows or industrial discharges that are point sources subject to permits under section 402 of the Federal Water Pollution Control Act, as amended (33 U.S.C. 1342), or source, special nuclear, or byproduct material as defined by the Atomic Energy Act of 1954, as amended (42 U.S.C. 2014).”

Subpart CCCC refers to “solid waste” as defined in 40 CFR 241.2, which refers to 40 CFR 258.2. 40 CFR 258.2 defines to *“means any garbage, or refuse, sludge from a wastewater treatment plant, water supply treatment plant, or air pollution control facility and other discarded material, including solid, liquid, semi-solid, or contained gaseous material resulting from industrial, commercial, mining, and agricultural operations, and from community activities, but does not include solid or dissolved materials in domestic sewage, or solid or dissolved materials in irrigation return flows or industrial discharges that are point sources subject to permit under 33 U.S.C. 1342, or source, special nuclear, or by-product material as defined by the Atomic Energy Act of 1954, as amended (68 Stat. 923).”*

Subparts AAAA do not define “solid waste” or reference waste as determined under 40 CFR 241. This subpart defines *“municipal solid waste or municipal-type solid waste”*

“means household, commercial/retail, or institutional waste. Household waste includes material discarded by residential dwellings, hotels, motels, and other similar permanent or temporary housing. Commercial/retail waste includes material discarded by stores, offices, restaurants, warehouses, nonmanufacturing activities at industrial facilities, and other similar establishments or facilities. Institutional waste includes materials discarded by schools, by hospitals (nonmedical), by nonmanufacturing activities at prisons and government facilities, and other similar establishments or facilities. Household, commercial/retail, and institutional waste does include yard waste and refuse-derived fuel. Household, commercial/retail, and institutional waste does not include used oil; sewage sludge; wood pallets; construction, renovation, and demolition wastes (which include railroad ties and telephone poles); clean wood; industrial process or manufacturing wastes; medical waste; or motor vehicles (including motor vehicle parts or vehicle fluff).”

Both of these definitions, "solid waste" and "municipal solid waste", contain the phrase "*other discarded materials*". Therefore, a waste determination must be conducted on the plastic feedstock to be introduced into the pyrolysis trains in accordance with 40 CFR 241.3.

The concern the DAQ has with the plastic feedstock is that EGG did not generate the plastic feedstock and thus, the original end user and/or generator had discarded this plastic material at some point.

Second Question: If the plastic feedstock is determined to be fuel or ingredients in accordance with 40 CFR 241.3, then would the EGG pyrolysis trains be exempt from Section 129 of the CAA (e.g. subject to Subpart AAAA, CCCC, or Subpart EEEE)?

Initially, the DAQ does not believe the pyrolysis trains, (e.g., engines and process heaters) would be subject to Section 129 and therefore Subparts AAAA, CCCC and EEEE would not be applicable to EGG's emission units.

Given the plastic material was discarded by the original end user or generator, the initial waste determination only pertains to the cracking/decomposition of plastic feedstock from the pyrolysis trains and all streams exiting the pyrolysis train should be re-evaluated in accordance with 40 CFR 241.3.

This is the real question: Would EGG need to conduct a waste determination for each of the exiting streams from the pyrolysis trains (e.g., "tars", "oil", "ash and char", and "synthetic gas") in accordance with 40 CFR 241.3?

The definition of "*solid waste*" at 40 CFR 258.a states,

"Solid waste means any garbage, or refuse, sludge from a wastewater treatment plant, water supply treatment plant, or air pollution control facility and other discarded material, including solid, liquid, semi-solid, or contained gaseous material resulting from industrial, commercial, mining, and agricultural operations, and from community activities, but does not include solid or dissolved materials in domestic sewage, or solid or dissolved materials in irrigation return flows or industrial discharges that are point sources subject to permit under 33 U.S.C. 1342, or source, special nuclear, or by-product material as defined by the Atomic Energy Act of 1954, as amended (68 Stat. 923)."

Thus, the DAQ does not believe that EGG's cleaned synthetic gas would need to be evaluated because the gas is not stored in a container. EGG's process consumes the synthetic gas as fuel to provide process heat for their process and generates electricity for the facility.

Third Question: EGG plans to route the ash and char stream to the vitrifier (process heater) to be oxidized into products of combustion. Would the vitrifier be subject to Subpart CCCC or EEEE?

The raw synthetic gas generated will exit the pyrolysis train through off-take with the ash and fixed carbon being collected in a deceleration chamber. The ash and fixed carbon, which is also referred to as "char", will be injected into the vitrifier. The vitrifier is best described as a retort or process heater with the purpose of providing process heat for the respective pyrolysis train. In the process description in EGG's modification application, the high temperatures in the vitrifier should be above the eutectic temperature of the ash and char to be combusted into CO₂ and H₂O.

The DAQ believes the synthetic gas stream and tar stream should be considered a fuel and the chlorine/chloride stream a raw ingredient for the production of hydrochloric acid. However, the injection of the ash and char into the vitrifiers should be viewed as incineration. The question is: because EGG generated the ash and char, would the vitrifiers be subject to Subpart CCCC as a CISWI unit.

The DAQ does not believe that the vitrifiers could be classified as an OWSI unit because the Follansbee facility is not an institutional facility generating this waste and the initial plastic feedstock does not meet the definition of "municipal solid waste." Therefore, based on the definitions under 40 CFR 60.2977 the vitrifier(s) is not an "other solid waste incineration unit".

Furthermore, the DAQ does not believe that EGG's vitrifiers qualify for any of the exclusions in Subpart CCCC (e.g. cogeneration facilities, small power production facilities).

Fourth Question, Would the vitrifiers be considered an "energy recovery unit" or a "commercial and industrial solid waste incineration unit" under Subpart CCCC?

The vitrifiers are required to provide process heat for the pyrolysis units with the exhaust used to dry the incoming plastic feedstock of excess moisture in the dryer section. EGG plans to use the generated "tars" and "cleaned synthetic gas" as fuels for the vitrifiers.

If EGG elected not to oxidize the ash and char stream in the vitrifiers (i.e. send the ash & char off-site for proper disposal), then would the vitrifiers be subject to Subpart CCCC?


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To aid you and your staff in this determination, a redacted copy of EGG's modification application is attached. The DAQ's permit file for R13-3555, EGG's application on processing medical waste using pyrolysis, can be viewed in our Application Xtender at:
<https://documents.dep.wv.gov/AppXtender/DataSources/DEPAX16/account/login?ret=Lw==>.

Instructions on using our Application Xtender are located at:
<https://dep.wv.gov/Data/Documents/AX-Instructions.pdf>.

Should you need to discuss this matter further, please do not hesitate to contact me by email at edward.s.andrews@wv.gov or phone at 304-926-0499 extension 41244..

Sincerely,
**Edward S.
Andrews, P.E.**
Edward S. Andrews, P.E.
Engineer

 Digitally signed by: Edward S. Andrews, P.E.
DN: CN = Edward S. Andrews, P.E. email =
edward.s.andrews@wv.gov C = AD O =
WVDEP/Division of Air Quality OU = Permitting
Date: 2024.03.06 14:38:41 -05'00'

cc:
Laura Crowder, Director, WV DAQ
Beverly McKeone, NSR Program Manager, WV DAQ
MaryCate Oplia, opila.marycate@epa.gov
Gwendolyn Supplee, Supplee.Gwendolyn@epa.gov

HCI Discussion 3/1/2024

Wednesday, March 27, 2024 1:38 PM



Andrews, Edward S <edward.s.andrews@wv.gov>

RE: Empire Discussion

1 message

Wood, Katie <katie.wood@tetrattech.com>
To: "Andrews, Edward S" <edward.s.andrews@wv.gov>
Cc: Farley Wood <fwood@empirede.com>

Fri, Mar 1, 2024 at 10:23 AM

Ed,

We have some answers to your questions below in red. Please let me know if you would like to discuss.

Thanks,

Katie

From: Andrews, Edward S <edward.s.andrews@wv.gov>
Sent: Friday, February 23, 2024 2:24 PM
To: Wood, Katie <katie.wood@tetrattech.com>; Farley Wood <fwood@empirede.com>
Subject: Re: Empire Discussion

⚠ CAUTION: This email originated from an external sender. Verify the source before opening links or attachments.



Using Chlorine gas and water reaction to produce HCl also produces a by-product of HOCl (hypochlorous acid). <https://www.bing.com/search?q=chlorine+gas+water+reaction&q=UT&pq=chlorine+gas+water+reaction&sc=10-27&cvid=1D306673308642F9BCEE5D950B9BFB08&FORM=QBRE&sp=1&ghc=1&lq=0> The process does not produce any Chlorine gas, it produces Chloride gas so no HOCL is produced. I have attached a paper provided by Technotherm for further information

Question is: Will Empire separate hypochlorous acid from the HCl or send it out as it? As per above no HOCL will be produced

Will the emissions of HCl go through a separate release point than the RTO stack? If it is a separate stack, I need the stack id and stack parameters of this point. No all emissions will go through the RTO

Also, I will need the calculations to support your emission estimate of HCl and concentration of HCl in the effluent release to the atmosphere from the production/storage/loading out of HCl. Calculations attached, these were included in the last submittal

Ed

On Thu, Feb 22, 2024 at 1:00 PM Wood, Katie <katie.wood@tetrattech.com> wrote:

Microsoft Teams meeting

Join on your computer, mobile app or room device

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Meeting ID: 248 808 531 032

Passcode: Gbfah4

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Edward Andrews, P.E.

Engineer

WVDEP/Division of Air Quality

304-926-0499 Ext 41244

[601 57th Street, SE](#)

[Charleston, WV 25304](#)



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KINETIC STUDY OF THERMAL DE-CHLORINATION OF PVC-CONTAINING WASTE

A. Castro^{1,2,a}, C. Carneiro¹, C. Vilarinho², D. Soares², C. Mações³, C. Sousa³ and F. Castro²

¹ CVR - Centre for Waste Valorization, Guimarães, Portugal

² CT2M - Centre for Mechanical and Materials Technologies, Mechanical Engineering Department, University of Minho, Guimarães, Portugal

³ Endutex - textile coatings, SA

^a acastro@cvresiduos.pt

ABSTRACT

With the increasing of plastics content in solid waste, both municipal and industrial, also increases the interest in its use as an energy source.

Some of these wastes are an important potential source of energy and might be valorized using the pyrolysis or gasification processes. However, the presence of high chlorine contents in its composition prevents its management by a thermal process, as consequence of toxic compounds production and their release to the atmosphere.

The present work asses a possible process for treating PVC-containing wastes in an environmentally friendly way. It is based on the effective de-chlorination of PVC-containing wastes through a pyrolysis process at low temperature before the carbonaceous residue from PVC-containing wastes being subject to a subsequent thermal treatment for energetic valorization.

Keywords: Pyrolysis, thermal degradation, PVC-containing waste, energy valorization;

INTRODUCTION

The presence of organic compounds on wastes, especially plastics, is considered an important source of energy. However, most of these plastics contain polyvinyl chloride (PVC), causing recycling problems when it is considered a thermal valorization process for its treatment [1], preventing the use of those residues on these processes, which main goal is the energy recovery [2,3]. A possible solution is to remove the chlorine from PVC-containing waste through a pyrolysis process before being subjected to a thermal treatment, for energetic valorization.

Pyrolysis is one of the applied techniques for energetic valorization and is defined as a process of irreversible chemical modification of compounds under the action of heat and in the absence of oxygen, causing thermal degradation [1]. The reaction involved in this process is endothermic and the characteristics of the obtained products are function of the waste composition and of several operating factors, such as the temperature, pressure and residence time in the pyrolysis reactor.

The pyrolysis process is considered by several authors [2 - 8] as a possible technique for the

operating factors, such as the temperature, pressure and residence time in the pyrolysis reactor.

The pyrolysis process is considered by several authors [2 - 8] as a possible technique for the energy recovery from PVC-containing wastes, through the thermal degradation of the chlorine

molecule. PVC pyrolysis involves significant cross-linked reactions with the formation of polyaromatic structures (possibly chlorinated) and a carbonaceous residue (char) [9]. Thus, it is possible to break down this molecule, allowing the chlorine recovery as hydrochloric acid or chloride [10], with potential economic gains.

However, the presence of poly(vinyl chloride) in wastes composition confines their management by thermal valorization processes as consequence of environmental problems and corrosion of the equipment. In fact, high levels of chlorine in wastes composition are responsible for the formation of hydrochloric acid, chlorine gas and dioxins [11]. Therefore, a preview thermal treatment by a pyrolysis process to remove the chlorine from PVC-containing wastes will be a suitable step if done prior to an energy recovery process to produce a synthesis gas.

Considering thermogravimetric analysis, it is assumed that the degradation of PVC occurs between 200 and 400 °C [2, 12]. At 250 °C, the decomposition of PVC has already been initiated, reaching a maximum at approximately 300 °C. At 350 °C the amount of chlorine present in PVC waste is less than 0.1%, which means that at this temperature, 99.5% of the whole chlorine has already been released [2]. At the end of the process of chlorine removal, a residual amount of chlorine remains on the waste [9].

The C-Cl bonds in the structure of PVC have a relatively lower binding energy than the C-C and C-H bonds, which justifies that the bonds of chlorine are the first to be broken, thus starting the thermal degradation of PVC. The de-chlorination of PVC is a free radicals chain reaction therefore requiring low activation energy to start, occurring at low temperatures [4, 7].

De-chlorination of PVC wastes is a mandatory step for any treatment process, able to recover energy from these wastes. In fact, from the decomposition of PVC, one polymeric fraction can be obtained with high energetic value:



As a matter of fact, products from the decomposition will be of the type C_nH_n .

This work aims the contemplation of new valorization processes and use of PVC-containing wastes. For the PVC molecule de-chlorination, tests were performed at low temperature pyrolysis and subsequent gasification of the remaining fraction in order to produce a synthesis gas with high energetic potential.

EXPERIMENTAL WORK

In this work, the kinetics of thermal de-chlorination has been studied, by simultaneous DTA/TGA determinations, under inert atmosphere. With all the experimental data obtained a multivariate

In this work, the kinetics of thermal de-chlorination has been studied, by simultaneous DTA/TGA determinations, under inert atmosphere. With all the experimental data obtained a multivariate regression of $\ln(r)$ has been performed in function of $1/T$ and $\ln([HCl])$. The kinetic model has been calculated just for points where temperature was lower than 340 °C, and the obtained model is:

$$\ln r = 31,3 - \frac{16100}{T} + 1,020 \ln[HCl]$$

with $r^2 = 0,9912$

This allows considering that reaction as a first order one with activation energy of 133800 J/mol \pm 760 J/mol.

For the kinetic study, a DTA/TGA (SDT 2960 from TA Instruments) testing at different temperatures has been carried out in order to determine the relationship between the rate of PVC de-chlorination and the temperature of the thermal treatment, under an inert atmosphere. It was used a commercial pure PVC powder with the chemical formula C_2H_3Cl , in which 56,7% is chlorine. The reference is VICIR S 950 and it is a vinyl chloride homopolymer produced by a suspension polymerization process.

Experiments have conducted up to 5 different maximum temperatures: 250, 275, 300, 325 and 400 °C, with a heating rate of 10 °C per minute until the desired temperature is reached. After reaching this temperature, a stage has been done during 360 minutes. Heat flux (weight corrected heat flow in W/g) and weight of sample, has been continuously recorded.

DTA/TGA testing performed indicates that the temperature of 340 °C enables the removal of 88 % of the chlorine present in the PVC material. The resulting de-chlorinated fraction, carbonaceous residue, has also been characterized and it is mainly constituted by carbon. This carbonaceous residue was testing up to 500°C in DTA/DTA and was verified that the combustion reaction of the carbonaceous material is complete at 493°C demonstrating potential as a fuel source to a following gasification in order to produce a synthesis gas with high energetic potential.

To characterize the sample of PVC used and the carbonaceous residue formed, it has been used an TruSpec Elemental Determinator, model TruSpec CHN, of Leco with a burn time of 452 seconds and an Philips Analytical sequential X-ray fluorescence (XRF) Spectrometer model X'Unique II.

Table 1. Comparison between the chemical composition (in wt%) of PVC sample used and the carbonaceous residue obtained from pyrolysis at 340 °C.

	PVC (initial sample)	PVC (Carbonaceous residue)
Carbon	38,4	89
Hydrogen	4,0	7
Chlorine	56,7	4

	(initial sample)	(Carbonaceous residue)
Carbon	38,4	89
Hydrogen	4,9	7
Chlorine	56,7	0,07

Through table 1, we are able to conclude that the de-chlorinated fraction obtained at 340°C is mainly constituted by carbon presenting residual chlorine content, 0,07 %.

Tests were performed in the laboratory and pilot scale, where the variables temperature, pressure and residence time inside the reactor were studied, as well as its influence on the reaction products obtained.

The pilot plant consists in a reactor where the pyrolysis occurs, with a stainless steel body heated by electrical resistance and a column of water where the gas is bubbled, as exemplified in figure 1. Measuring instruments such as thermocouples and pressure gauges are used to control the conditions (temperature and pressure) inside the reactor.

The fixation of the released chlorine is obtained by water absorption, forming HCl (hydrochloric acid), CaCl₂ (calcium chloride) and also NaCl (sodium chloride), when the aqueous solution, containing CaO (calcium oxide) or NaOH (sodium hydroxide), respectively.

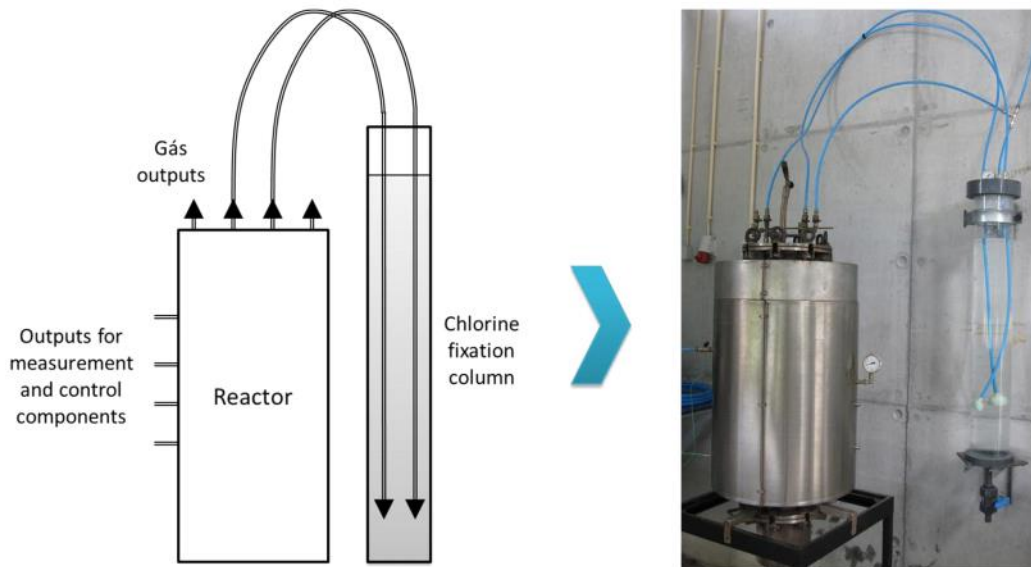


Figure 1: Scheme of pilot scale used for the tests.

Initially, a slight vacuum is created to remove the oxygen inside the reactor, then the test is initiated and divided into two stages. The first stage is a low-temperature pyrolysis or carbonization, where the de-chlorination of the PVC-containing waste reaction occurs, the released chlorine is recovered in the column in the form of hydrochloric acid, sodium chloride, or calcium chloride. After the first

initially, a slight vacuum is created to remove the oxygen inside the reactor, then the test is initiated and divided into two stages. The first stage is a low-temperature pyrolysis or carbonization, where the de-chlorination of the PVC-containing waste reaction occurs, the released chlorine is recovered in the column in the form of hydrochloric acid, sodium chloride or calcium chloride. After the first stage is completed, second stage, takes place, then the carbonaceous residue (without chlorine) resulting from the first stage, is energetically valorized, at temperatures above 550 ° C.

The residence time in the reactor was tested by the pressure differences, viewed through the pressure gauge in the reactor. Thus, the reaction starts in vacuum and is assumed as completed when the pressure reaches zero, i.e. atmospheric pressure. During the reaction, when the pressure is 0,5 bar above atmospheric pressure, it is enough for the syngas formed inside the reactor can bubble in column. After all the gas is released, then the pressure drops to zero on the gauge, i.e., atmospheric pressure, thus giving the information that the reaction is complete.

All materials used in building a pilot plant must be well chosen, because of corrosion of materials and isolation. The absence of leakage or entry of gases must also be controlled, since the produced gases are toxic and cannot leak to the atmosphere, and also because as pyrolysis is a process that must take place in anoxic environment, thus it should be affected by any entry of oxidizing agents.

The main reaction product is a synthesis gas for burning to produce heat.

CONCLUSIONS

In this work, the kinetics of the reaction of thermal decomposition of PVC were studied, leading to the development of a kinetic model, with the expression $\ln r = 31,3 - 16100/T + 1,020 \ln C (HCl)$. This model was obtained for the decomposition temperatures lower than 340 °C, in which almost all chlorine is removed from the pure PVC through the chemical reaction described, with an activation energy of 133800 J/mol, value very close to the one obtained by others researchers [4].

The kinetic model was verified in laboratorial trials, and it was observed a reduction of 88 % of the chlorine contained in PVC, making it suitable to be used in a recovery process to obtain a synthesis gas.

During the pyrolysis treatment, released chlorine can be fixed in the form of aqueous solution of hydrochloric acid, calcium chloride or sodium chloride. This process shall constitute an attractive route, envisaging environmental benefits, thereby avoiding deleterious effects of toxic gas emissions.

In this study, we propose a methodology to remove chlorine from PVC-containing wastes allowing the valorization of the chlorine-free remaining fraction. A double benefit can thus be achieved as it not only saves the cost of landfilling but also produces an value added syngas.

It is concluded that for PVC-containing waste, the solution can pass through a full treatment

not only saves the cost of landfilling but also produces an value added syngas.

It is concluded that for PVC-containing waste, the solution can pass through a full treatment consisting of two phases. Where the first is to remove the chlorine from the PVC molecule and the second is to valorize the remaining fraction.

References

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HCl Production Questions 3/1/2024

Wednesday, March 6, 2024 1:48 PM



Andrews, Edward S <edward.s.andrews@wv.gov>

RE: Empire Discussion

1 message

Wood, Katie <katie.wood@tetrattech.com>
To: "Andrews, Edward S" <edward.s.andrews@wv.gov>
Cc: Farley Wood <fwood@empirede.com>

Fri, Mar 1, 2024 at 10:23 AM

Ed,

We have some answers to your questions below in red. Please let me know if you would like to discuss.

Thanks,

Katie

From: Andrews, Edward S <edward.s.andrews@wv.gov>
Sent: Friday, February 23, 2024 2:24 PM
To: Wood, Katie <katie.wood@tetrattech.com>; Farley Wood <fwood@empirede.com>
Subject: Re: Empire Discussion

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Using Chlorine gas and water reaction to produce HCl also produces a by-product of HOCl (hypochlorous acid). <https://www.bing.com/search?q=chlorine+gas+water+reaction&q=UT&pq=chlorine+gas+water+reaction&sc=10-27&cvid=1D306673308642F9BCEE5D950B9BFB08&FORM=QBRE&sp=1&ghc=1&lq=0> The process does not produce any Chlorine gas, it produces Chloride gas so no HOCL is produced. I have attached a paper provided by Technotherm for further information

Question is: Will Empire separate hypochlorous acid from the HCl or send it out as it? As per above no HOCL will be produced

Will the emissions of HCl go through a separate release point than the RTO stack? If it is a separate stack, I need the stack id and stack parameters of this point. No all emissions will go through the RTO

Also, I will need the calculations to support your emission estimate of HCl and concentration of HCl in the effluent release to the atmosphere from the production/storage/loading out of HCl. Calculations attached, these were included in the last submittal

Ed

On Thu, Feb 22, 2024 at 1:00 PM Wood, Katie <katie.wood@tetrattech.com> wrote:

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Edward Andrews, P.E.

Engineer

WVDEP/Division of Air Quality

304-926-0499 Ext 41244

[601 57th Street, SE](#)

[Charleston, WV 25304](#)



KINETIC STUDY OF THERMAL DE-CHLORINATION OF PVC-CONTAINING WASTE.pdf

248K



KINETIC STUDY OF THERMAL DE-CHLORINATION OF PVC-CONTAINING WASTE

A. Castro^{1,2,a}, C. Carneiro¹, C. Vilarinho², D. Soares², C. Mações³, C. Sousa³ and F. Castro²

¹ CVR - Centre for Waste Valorization, Guimarães, Portugal

² CT2M - Centre for Mechanical and Materials Technologies, Mechanical Engineering Department, University of Minho, Guimarães, Portugal

³ Endutex - textile coatings, SA

^a acastro@cvresiduos.pt

ABSTRACT

With the increasing of plastics content in solid waste, both municipal and industrial, also increases the interest in its use as an energy source.

Some of these wastes are an important potential source of energy and might be valorized using the pyrolysis or gasification processes. However, the presence of high chlorine contents in its composition prevents its management by a thermal process, as consequence of toxic compounds production and their release to the atmosphere.

The present work assesses a possible process for treating PVC-containing wastes in an environmentally friendly way. It is based on the effective de-chlorination of PVC-containing wastes through a pyrolysis process at low temperature before the carbonaceous residue from PVC-containing wastes being subject to a subsequent thermal treatment for energetic valorization.

Keywords: Pyrolysis, thermal degradation, PVC-containing waste, energy valorization;

INTRODUCTION

The presence of organic compounds on wastes, especially plastics, is considered an important source of energy. However, most of these plastics contain polyvinyl chloride (PVC), causing recycling problems when it is considered a thermal valorization process for its treatment [1], preventing the use of those residues on these processes, which main goal is the energy recovery [2,3]. A possible solution is to remove the chlorine from PVC-containing waste through a pyrolysis process before being subjected to a thermal treatment, for energetic valorization.

Pyrolysis is one of the applied techniques for energetic valorization and is defined as a process of irreversible chemical modification of compounds under the action of heat and in the absence of oxygen, causing thermal degradation [1]. The reaction involved in this process is endothermic and the characteristics of the obtained products are function of the waste composition and of several operating factors, such as the temperature, pressure and residence time in the pyrolysis reactor.

The pyrolysis process is considered by several authors [2 - 8] as a possible technique for the energy recovery from PVC-containing wastes, through the thermal degradation of the chlorine

The pyrolysis process is considered by several authors [2 - 8] as a possible technique for the energy recovery from PVC-containing wastes, through the thermal degradation of the chlorine

molecule. PVC pyrolysis involves significant cross-linked reactions with the formation of polyaromatic structures (possibly chlorinated) and a carbonaceous residue (char) [9]. Thus, it is possible to break down this molecule, allowing the chlorine recovery as hydrochloric acid or chloride [10], with potential economic gains.

However, the presence of poly(vinyl chloride) in wastes composition confines their management by thermal valorization processes as consequence of environmental problems and corrosion of the equipment. In fact, high levels of chlorine in wastes composition are responsible for the formation of hydrochloric acid, chlorine gas and dioxins [11]. Therefore, a previous thermal treatment by a pyrolysis process to remove the chlorine from PVC-containing wastes will be a suitable step if done prior to an energy recovery process to produce a synthesis gas.

Considering thermogravimetric analysis, it is assumed that the degradation of PVC occurs between 200 and 400 °C [2, 12]. At 250 °C, the decomposition of PVC has already been initiated, reaching a maximum at approximately 300 °C. At 350 °C the amount of chlorine present in PVC waste is less than 0.1%, which means that at this temperature, 99.5% of the whole chlorine has already been released [2]. At the end of the process of chlorine removal, a residual amount of chlorine remains on the waste [9].

The C-Cl bonds in the structure of PVC have a relatively lower binding energy than the C-C and C-H bonds, which justifies that the bonds of chlorine are the first to be broken, thus starting the thermal degradation of PVC. The de-chlorination of PVC is a free radicals chain reaction therefore requiring low activation energy to start, occurring at low temperatures [4, 7].

De-chlorination of PVC wastes is a mandatory step for any treatment process, able to recover energy from these wastes. In fact, from the decomposition of PVC, one polymeric fraction can be obtained with high energetic value:



As a matter of fact, products from the decomposition will be of the type C_nH_n .

This work aims the contemplation of new valorization processes and use of PVC-containing wastes. For the PVC molecule de-chlorination, tests were performed at low temperature pyrolysis and subsequent gasification of the remaining fraction in order to produce a synthesis gas with high energetic potential.

EXPERIMENTAL WORK

In this work, the kinetics of thermal de-chlorination has been studied, by simultaneous DTA/TGA determinations, under inert atmosphere. With all the experimental data obtained a multivariate regression of $\ln(r)$ has been performed in function of $1/T$ and $\ln([\text{HCl}])$. The kinetic model has been calculated just for points where temperature was lower than 340 °C, and the obtained model is:

regression of $\ln(r)$ has been performed in function of $1/T$ and $\ln([HCl])$. The kinetic model has been calculated just for points where temperature was lower than 340 °C, and the obtained model is:

$$\ln r = 31,3 - \frac{16100}{T} + 1,020 \ln[HCl]$$

with $r^2 = 0,9912$

This allows considering that reaction as a first order one with activation energy of 133800 J/mol \pm 760 J/mol.

For the kinetic study, a DTA/TGA (SDT 2960 from TA Instruments) testing at different temperatures has been carried out in order to determine the relationship between the rate of PVC de-chlorination and the temperature of the thermal treatment, under an inert atmosphere. It was used a commercial pure PVC powder with the chemical formula C_2H_3Cl , in which 56,7% is chlorine. The reference is VICIR S 950 and it is a vinyl chloride homopolymer produced by a suspension polymerization process.

Experiments have conducted up to 5 different maximum temperatures: 250, 275, 300, 325 and 400 °C, with a heating rate of 10 °C per minute until the desired temperature is reached. After reaching this temperature, a stage has been done during 360 minutes. Heat flux (weight corrected heat flow in W/g) and weight of sample, has been continuously recorded.

DTA/TGA testing performed indicates that the temperature of 340 °C enables the removal of 88 % of the chlorine present in the PVC material. The resulting de-chlorinated fraction, carbonaceous residue, has also been characterized and it is mainly constituted by carbon. This carbonaceous residue was testing up to 500°C in DTA/DTA and was verified that the combustion reaction of the carbonaceous material is complete at 493°C demonstrating potential as a fuel source to a following gasification in order to produce a synthesis gas with high energetic potential.

To characterize the sample of PVC used and the carbonaceous residue formed, it has been used an TruSpec Elemental Determinator, model TruSpec CHN, of Leco with a burn time of 452 seconds and an Philips Analytical sequential X-ray fluorescence (XRF) Spectrometer model X'Unique II.

Table 1. Comparison between the chemical composition (in wt%) of PVC sample used and the carbonaceous residue obtained from pyrolysis at 340 °C.

	PVC (initial sample)	PVC (Carbonaceous residue)
Carbon	38,4	89
Hydrogen	4,9	7
Chlorine	56,7	0,07

Through table 1, we are able to conclude that the de-chlorinated fraction obtained at 340°C is mainly constituted by carbon presenting residual chlorine content, 0,07 %.

Tests were performed in the laboratory and pilot scale, where the variables temperature, pressure and residence time inside the reactor were studied, as well as its influence on the reaction products obtained.

The pilot plant consists in a reactor where the pyrolysis occurs, with a stainless steel body heated by electrical resistance and a column of water where the gas is bubbled, as exemplified in figure 1. Measuring instruments such as thermocouples and pressure gauges are used to control the conditions (temperature and pressure) inside the reactor.

The fixation of the released chlorine is obtained by water absorption, forming HCl (hydrochloric acid), CaCl₂ (calcium chloride) and also NaCl (sodium chloride), when the aqueous solution, containing CaO (calcium oxide) or NaOH (sodium hydroxide), respectively.

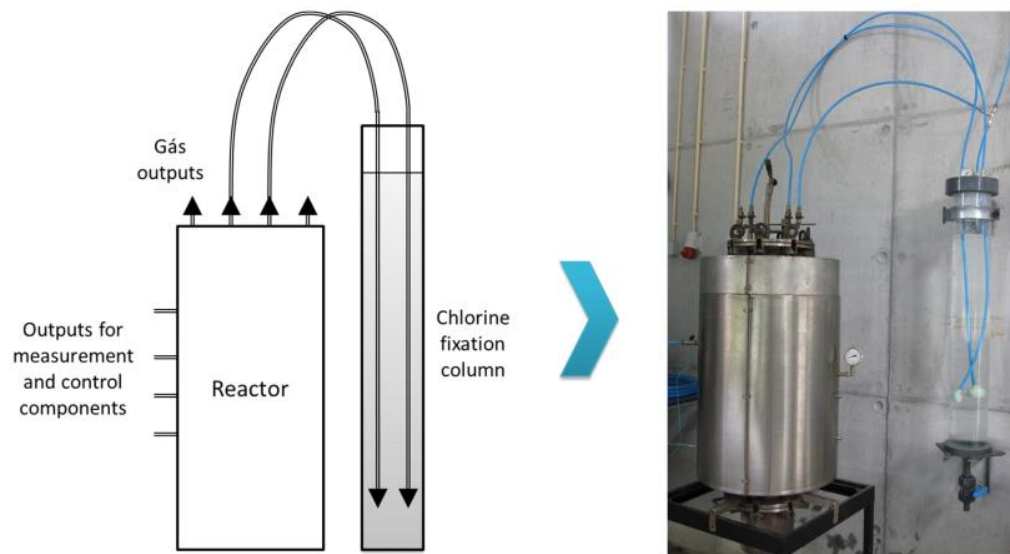


Figure 1: Scheme of pilot scale used for the tests.

Initially, a slight vacuum is created to remove the oxygen inside the reactor, then the test is initiated and divided into two stages. The first stage is a low-temperature pyrolysis or carbonization, where the de-chlorination of the PVC-containing waste reaction occurs, the released chlorine is recovered in the column in the form of hydrochloric acid, sodium chloride or calcium chloride. After the first stage is completed, second stage, takes place, then the carbonaceous residue (without chlorine) resulting from the first stage, is energetically valorized, at temperatures above 550 °C.

The residence time in the reactor was tested by the pressure differences, viewed through the pressure gauge in the reactor. Thus, the reaction starts in vacuum and is assumed as completed when the pressure reaches zero. i.e. atmospheric pressure. During the reaction. when the pressure

The residence time in the reactor was tested by the pressure differences, viewed through the pressure gauge in the reactor. Thus, the reaction starts in vacuum and is assumed as completed when the pressure reaches zero, i.e. atmospheric pressure. During the reaction, when the pressure is 0,5 bar above atmospheric pressure, it is enough for the syngas formed inside the reactor can bubble in column. After all the gas is released, then the pressure drops to zero on the gauge, i.e., atmospheric pressure, thus giving the information that the reaction is complete.

All materials used in building a pilot plant must be well chosen, because of corrosion of materials and isolation. The absence of leakage or entry of gases must also be controlled, since the produced gases are toxic and cannot leak to the atmosphere, and also because as pyrolysis is a process that must take place in anoxic environment, thus it should be affected by any entry of oxidizing agents.

The main reaction product is a synthesis gas for burning to produce heat.

CONCLUSIONS

In this work, the kinetics of the reaction of thermal decomposition of PVC were studied, leading to the development of a kinetic model, with the expression $\ln r = 31,3 - 16100/T + 1,020 \ln C (HCl)$. This model was obtained for the decomposition temperatures lower than 340 °C, in which almost all chlorine is removed from the pure PVC through the chemical reaction described, with an activation energy of 133800 J/mol, value very close to the one obtained by others researchers [4].

The kinetic model was verified in laboratorial trials, and it was observed a reduction of 88 % of the chlorine contained in PVC, making it suitable to be used in a recovery process to obtain a synthesis gas.

During the pyrolysis treatment, released chlorine can be fixed in the form of aqueous solution of hydrochloric acid, calcium chloride or sodium chloride. This process shall constitute an attractive route, envisaging environmental benefits, thereby avoiding deleterious effects of toxic gas emissions.

In this study, we propose a methodology to remove chlorine from PVC-containing wastes allowing the valorization of the chlorine-free remaining fraction. A double benefit can thus be achieved as it not only saves the cost of landfilling but also produces an value added syngas.

It is concluded that for PVC-containing waste, the solution can pass through a full treatment consisting of two phases. Where the first is to remove the chlorine from the PVC molecule and the second is to valorize the remaining fraction.

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- [11] Kamo T., Yamamoto Y., Miki K., Sato Y. Conversion of waste polyvinyl chloride (PVC) to useful chemicals. (1996) *Resources and Environment*. 305, Japan.
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HCl Spec

Friday, February 23, 2024 4:18 PM

Product Specifications

luriatic Acid, 20 DEG Baume (HCL 32)

Item	Specification
	APHA
Color, Max	15.0
Degrees Baume DEG Baume @60F	20.0-20.8
	Parts Per Million
Arsenic, Max (AS)	0.1
Bromide, Max (BR)	50.0
Calcium, Max (CA)	2.0
Free Chlorine, Max (CL2)	3.0
Fluoride, Max (F)	2.0
Iron, Max (FE)	0.5
Non-Volatile Residue, Max (NVR)	15.0
Organics, Max	1.0
Lead, Max (PB)	0.2
Sulfate, Max	10.0
	Percent by Weight
Hydrogen Chloride	31.5-32.9

Approved 07.12.1996

Response to HCl questions 2/21/2024

Wednesday, February 21, 2024 8:49 AM



Andrews, Edward S <edward.s.andrews@wv.gov>

FW: Empire's Revised Modification App

1 message

Wood, Katie <katie.wood@tetrattech.com>
To: Edward Andrews <edward.s.andrews@wv.gov>

Wed, Feb 21, 2024 at 8:33 AM

Ed,

Please see responses below for the HCL for the process. I will follow up on the plastic feedstock as fuel here shortly.

Thanks,

Katie

From: Farley R. Wood, P.E. <fwood@empirede.com>
Sent: Tuesday, February 20, 2024 2:14 PM
To: Wood, Katie <katie.wood@tetrattech.com>
Subject: RE: Empire's Revised Modification App

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Katie,

Please see below:



Farley R. Wood, P.E.
Vice President of Engineering

Main Office (304) 935-5851
Mobile: (304) 650-2023
Teams: [Click Here](#)

fwood@empirede.com
www.empirediversifiedenergy.com

From: Wood, Katie <katie.wood@tetrattech.com>
Sent: Tuesday, February 20, 2024 11:36 AM

To: Farley R. Wood, P.E. <fwood@empirede.com>
Subject: FW: Empire's Revised Modification App

You don't often get email from katie.wood@tetrattech.com. [Learn why this is important](#)

From: Andrews, Edward S <edward.s.andrews@wv.gov>
Sent: Tuesday, February 20, 2024 10:16 AM
To: Wood, Katie <katie.wood@tetrattech.com>
Subject: Re: Empire's Revised Modification App

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Katie,

I will need additional information about the HCl production/storage/loading out rack to develop the appropriate permit requirements.

How will the HCl be produced and at what concentration? **Absorption and cooling of chlorine gas into demineralized water in a spray tower. The target concentration of hydrochloric acid is 31.45% (20° Baume°).**

How much HCl be stored on site (identify the tanks and dimensions of the tanks)? **We will have two 10,305 gallon tanks for HCl storage. One for in spec HCl and one for out of spec HCL. Tank dimensions are 11' 11" diameter by 14' high.**

The goal is to make in spec product, so the out of spec tank will hopefully be nearly empty most of the time. We will have a 1,500 gallon production tank (7'2" diameter by 5' 11" high) witch will be where quality analysis samples are regularly taken.

Based on the analysis the HCl will be routed to the in spec or out of spec tanks. HCl will be removed from the tanks on a daily basis by FSTI, an onsite tenant of the Port. Production and shipments will be roughly equal to minimize stored product.

Is the proposed scrubber going to be used to control the storage and loadout racks or just the loading rack? **Both**

Will the pyrolysis units need to process feedstock that contains PVC (polyvinyl chloride) type of plastic material to produce HCl? **Yes, we have the ability to not produce HCl by keeping PVC out of the feed material.**

Also, the reference to House Bill 4048 does not help me justify why the plastic feedstock should be treated as fuel?

Specifically, I need sufficient information from the application to indicate the plastic feedstock is not considered waste and therefore the facility (pyrolysis units) are not subject to Subpart AAAA, CCCC, and Subpart EEEE because the feedstock material is not waste.

Ed

On Wed, Feb 7, 2024 at 8:55 AM Wood, Katie <katie.wood@tetrattech.com> wrote:

Thanks Ed,

Let me dive into this a little more and talk to them and I will reach out to discuss.

Thanks,

Katie

From: Andrews, Edward S <edward.s.andrews@wv.gov>

Sent: Tuesday, February 6, 2024 9:08 AM

To: Wood, Katie <katie.wood@tetrattech.com>

Subject: Empire's Revised Modification App

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Katie,

It is still unclear to me how HCl is going to be generated and separate from the pyrolysis process.

I am not sure if I can just accept WV House Bill 4048 as proof that the material being processed is non-waste.

I would like to discuss these issues further in the near future.

Ed

--

Edward Andrews, P.E.

Engineer

WVDEP/Division of Air Quality

304-926-0499 Ext 41244

[601 57th Street, SE](#)

[Charleston, WV 25304](#)

--

Edward Andrews, P.E.

Engineer

WVDEP/Division of Air Quality

304-926-0499 Ext 41244

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Notary Public 2/5/24

Monday, February 5, 2024 1:43 PM



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Questions or comments? Please contact us

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850-245-6500



Andrew, Edward S <edward.s.andrew@wv.gov>

RE: Incomplete App Email for Permit App R13-3555A

1 message

Wood, Katie <katie.wood@wvtech.com> Tue, Jan 23, 2024 at 4:28 PM
To: "Andrew, Edward S" <edward.s.andrew@wv.gov>
Cc: Beverly D Osborne <beverly.d.osborne@wv.gov>; Brian S Tophaback <brian.s.tophaback@wv.gov>; Eric Bernd <eric.bernd@wv.gov>; Kenneth Brown <kenneth.brown@wv.gov>; Tanya Wood <tanya.wood@wvtech.com>

Hi,
Please find attached the revised notification application for Empire Green Generation. Please find the response to your comments below in blue. Please don't hesitate to reach out if you have any questions.
Thank you.

Katie Wood | Environmental Scientist
Direct: +1 (248) 296-9662 | Mobile: +1 (248) 988-8889 | katie.wood@wvtech.com
Company: Pugh, Chase and Associates Group
Tara Tech | Lansing, MI | Science | Data
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From: Andrew, Edward S <edward.s.andrew@wv.gov>
Sent: Wednesday, December 20, 2023 2:34 PM
To: Edward Brown <edward.brown@wv.gov>; Tanya Wood <tanya.wood@wvtech.com>; Wood, Katie <katie.wood@wvtech.com>
Cc: Beverly D Osborne <beverly.d.osborne@wv.gov>; Brian S Tophaback <brian.s.tophaback@wv.gov>; Eric Bernd <eric.bernd@wv.gov>
Subject: Incomplete App Email for Permit App R13-3555A

CAUTION: This email originated from an external sender. Verify the source before opening links or attachments.

RE: Application Status: Incomplete
Empire Green Generation
Permit Application No. R13-3555A
Plant ID No. 889-00141

Hi Bevy:

Your application for a modification permit for a plastic recycling by pyrolysis facility was received by this Division on December 1, 2023, and assigned to the writer for review. Upon initial review of said application, it has been determined that the application as submitted is incomplete based on the following items:

1. Affidavit of Publication of Class I Legal Ad. Included in pdf
2. Discussion of the proposed physical changes, if applicable, and/or change to the method of operation. Specifically, the discussion needs to either outline or go into detail regarding proposed regulatory changes to the permit, if applicable; type and amount/weight of the plastic feedstock going to the process by the facility; any processing/pre-treating being going to be conducted on the plastic prior to being introduced into the pyrolysis vessel; if there processing to be going to occur off-site, it will need to be identified and discussed; a discussion how the facility will switch back and forth in processing medical waste and plastic feedstock, such a discussion why processing the proposed plastic feedstock is not viewed as waste disposal through incineration or the context of the Clean Air Act and how the criteria in a facility within the requirements and provisions of an EPA 241 - SOLID WASTES USED AS FUELS OR INCINERANTS IN COMBUSTION UNITS. The only physical change is the in feedstock, there is no change in the process. Additional information about the pre-processing handling was added to section C process description. There will be no switching back and forth of feedstock, the facility will only be recycling plastics. A discussion of the regulatory requirements has been added to section D regulatory discussion.
3. The plant (Attachment E) needs to be updated to identify emission units and emission points. Emission units include in pdf.pdf
4. Attachment J needs to be complete for each emission point. No additional emission points have been added
5. Attachment K and L need to be completed. The potential for leaking equipment (e.g., valves, pumps, compressors, emissions, pressure relief devices) needs to be quantified and discussed in these two attachments. Attachments completed and incorporated in PDF
6. Each of the subject pages that contain confidential business information (CBI) needs to be marked "redacted copy - claim of confidentiality" in accordance with 20CSR15.1.4. Redacted pages included in confiders

In addressing items 2 through 6 needs to be reflective within the redacted application as a single PDF file.

The emission estimates appear to be identical to the emission estimates for processing medical waste with the same process unit. Please review these estimates and review as necessary within permit unit. Why the estimates will not change given the change in feedstock. The estimates are not expected to change, the majority of the medical waste feedstock was anticipated to be plastics. There is not change to the process, just feedstock so the emission estimates remain the same.

Please advise the status of this application in writing by no later than January 19, 2024. Application review will not commence until the application has been deemed to be technically complete. Failure to respond to this request in a timely manner may result in the denial of the application.

Should you have any questions, please contact Ed Andrew at (248) 926-8899 ext. 41244 or reply to this email.

Edward Andrew, P.E.
Engineer
WDEP/Division of Air Quality
304-926-8889 Ext 41244
601 S 7th Street, SE
Chattanooga, WV 25924

R13-3555 Modification_Application_EGD - Redacted_Final Rev.pdf
2/24/24

NSR (45CSR13) APPLICATION FORM

 WEST VIRGINIA DEPARTMENT OF ENVIRONMENTAL PROTECTION DIVISION OF AIR QUALITY 815 17 th Street, SE Charleston, WV 25304 (304) 526-0400 www.deq.wv.gov		APPLICATION FOR NSR PERMIT AND TITLE V PERMIT REVISION (OPTIONAL)	
PLEASE CHECK ALL THAT APPLY TO THIS (45CSR13) (IF KNOWN) <input type="checkbox"/> CONSTRUCTION <input type="checkbox"/> MODIFICATION <input type="checkbox"/> RELOCATION <input type="checkbox"/> ADMINISTRATIVE AMENDMENT <input type="checkbox"/> MINOR MODIFICATION <input type="checkbox"/> CLASS - ADMINISTRATIVE UPDATE <input type="checkbox"/> TECHNOLOGY <input type="checkbox"/> IMPROVEMENT/REGISTRATION <input type="checkbox"/> CLASS - ADMINISTRATIVE UPDATE <input type="checkbox"/> AFTER THE FACT		PLEASE CHECK TYPE OF 45CSR13 (TITLE V) REVISION (IF ANY) <input type="checkbox"/> ADMINISTRATIVE AMENDMENT <input type="checkbox"/> MINOR MODIFICATION <input type="checkbox"/> IMPROVEMENT/REGISTRATION IF ANY SUCH ABOVE IS CHECKED, INCLUDE TITLE V REVISION INFORMATION IN ATTACHMENT 5 TO THIS APPLICATION	
FOR TITLE V FACILITIES ONLY: Please refer to "Title V Revision Checklist" in order to determine your Title V Revision update (Appendix A, "Title V Permit Revision Flowchart") and ability to proceed with the changes requested in this Permit Application.			
Section I - General			
1. Name of applicant (as registered with the WV Secretary of State's Office): Chapin Steel Separators, LLC		2. Federal Employer ID No. (FEIN): 00-3197000	
3. Name of facility (if different from above): Fuldaheim Coalmine		4. The applicant is the: <input type="checkbox"/> OWNER <input type="checkbox"/> OPERATOR <input type="checkbox"/> BOTH	
5A. Applicant's mailing address: 1480 Main Street, Fuldaheim, WV 26037		5B. Facility's present physical address: 881 Rogers Rd., Fuldaheim, WV 26037	
6. West Virginia Business Registration. Is the applicant a resident of the State of West Virginia? <input checked="" type="checkbox"/> YES <input type="checkbox"/> NO - If YES, provide a copy of the Certificate of Incorporation/Organization/Partnership (one page) including any name change amendments or other Business Registration Certificate as Attachment A. - If NO, provide a copy of the Certificate of Authority/Authority of L.L.C./Registration (one page) including any name change amendments or other Business Certificate as Attachment A.			
7. If applicant is a subsidiary corporation, please provide the name of parent corporation.			
8. Does the applicant own, lease, have an option to buy or otherwise have control of the proposed job? <input checked="" type="checkbox"/> YES <input type="checkbox"/> NO - If YES, please explain: Own and Operate			
9. If NO, you are not eligible for a permit for this source.			
10. Type of plant or facility (business sector) to be constructed, modified, relocated, administratively updated or temporarily permitted (e.g., coal processing plant, primary crusher, etc.): Plastic Recycling By Pyrolysis		11. North American Industry Classification System (NAICS) code for the facility: 382200	
11A. DQG Plant ID No. (for existing facilities only): 938-30141		11B. List all current 45CSR13 and 45CSR12 (Title V) permit numbers associated with this process (for existing facilities only): 813-0550	
All of the required forms and additional information can be found under the Permitting Section of D&E's website, or requested by phone.			

12A. For Modifications, Administrative Updates or Temporary permits at an existing facility, please provide directions to the present location of the facility from the nearest state road.
For Construction or Relocation permits, please provide directions to the proposed new site location from the nearest state road. Include a MAP in Attachment B.

Turn off of WV-2 onto Veterans Drive (2.6 miles). Turn right onto Rogers Road (0.2 miles). Facility location will be on the right.

12B. New site address (if applicable):	12C. Nearest city or town: Fuldaheim	12D. County: Boke
12E. UTM Northing (NM): 48-33866	12F. UTM Easting (EM): 46-85429	12G. UTM Zone: 17T

13. Briefly describe the proposed changes to the facility. The facility will be recycling plastics into pyrolysis (used as originally permitted).

14A. Provide the date of installation/modification or change: 10/2024
14B. Date of anticipated Start-Up (If a new job):
10/2024
If this is an After-the-Fact permit application, provide the date (and when) the proposed change will happen.

15. Provide a Schedule of the planned installation of Change to and Start-Up of each of the units proposed in this permit application in Attachment C (if more than one unit is involved).

16. Provide maximum permitted Operating Schedule of activity/facilities outlined in this application:
- operate the Day 24 - Operate the Week 2 - Operate the Year 2

17. Risk Management Plans. If the facility is subject to 112(b) of the 1990 CAA, or will become subject due to proposed changes the applicant may be asked to provide a Risk Management Plan (RMP) to U.S. EPA Region 8.
18. Is demolition or physical relocation at an existing facility involved? YES NO

19. Regulatory Discussion. List all Federal and State air pollution control regulations that you believe are applicable to the proposed process (if known). A list of possible applicable requirements is also included in Attachment 5 of this application (Title V Permit Revision Information). Discuss applicability and proposed demonstration of compliance of sources. Provide this information in Attachment D.

Section II - Additional attachments and supporting documents.

19. Include a check payable to WVDEP - Division of Air Quality with the appropriate application fee (per 45CSR22 and 45CSR23).

20. Include a Table of Contents as the first page of your application package.

21. Provide a Plot Plan, e.g. aerial map(s) (vector preferred) showing the location of the property on which the stationary emissions unit is to be located in Attachment E (Refer to Plot Plan Guidelines).
- Indicate the location of the nearest protected structures (e.g., church, school, business, residential).

22. Provide a Detailed Process Flow Diagram(s) showing each proposed or modified emissions unit, emission point and control device in Attachment F.

23. Provide a Process Description in Attachment G.
- Also describe and quantify to the extent possible all changes made to the facility since the last permit review (if applicable).

All of the required forms and additional information can be found under the Permitting Section of D&E's website, or requested by phone.

State of West Virginia

Certificate

I, Mac Warner, Secretary of State of the State of West Virginia, hereby certify that

EMPIRE GREEN GENERATION, LLC

was duly authorized under the laws of this state to transact business in West Virginia as a foreign limited liability company on December 09, 2021.

The company is filed as an at-will company, for an indefinite period.

I further certify that the company has not been revoked or administratively dissolved by the State of West Virginia nor has the West Virginia Secretary of State issued a Certificate of Cancellation or Termination to the company.

Accordingly, I hereby issue this Certificate of Authorization

CERTIFICATE OF AUTHORIZATION

Validation ID:8WV3R_YASBM

Given under my hand and the Great Seal of the State of West Virginia on this day of January 07, 2022

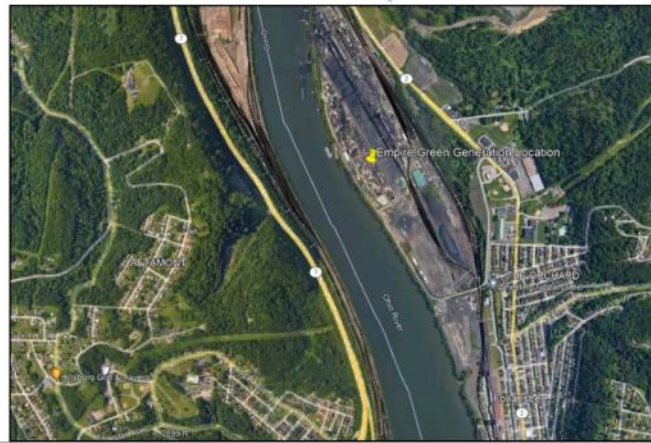


Mac Warner

Secretary of State

ATTACHMENT B

Maps



**EMPIRE GREEN GENERATION, LLC
FOLLANSBEE, WV
SITE MAP AND LAYOUT**

14

ATTACHMENT C
Installation and Startup Schedule

15



ATTACHMENT C: INSTALLATION AND START UP SCHEDULE

Unit	Start of Installation	Approximate Start of Operations
900 & 1000 (Thermal Oxidizer and Stack Exhaust)	October 2022	February 2024

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ATTACHMENT D

Regulatory Discussion

15

1.1 West Virginia State Requirements

The Facility will be a minor source of emissions under the NSR Program as well as the Title V Operating Permit program under §603C9-30. However, the potential uncontrolled emissions for the Facility will exceed the permitting threshold of 6 pounds per hour (lb/hr) and/or 144 pounds per day (lb/day) in accordance with WVDEP §603C9-3-2.4. Accordingly, Empire Green Generation, LLC is addressing this application for a minor source permit to install and operate.

In addition to regulations, state regulations that pertain to this Facility are listed in Table 1-1. Titles shown in capital letters in the table are permits, notifications, and/or reports that will be needed for construction and operation of the Facility.

Federal authority is delegated to the State of West Virginia, and all permit applications will be submitted to West Virginia Department of Environmental Protection (WVDEP). The following list of air permits is applicable to the proposed facility:

Table 1-1 West Virginia DEP Applicable Regulations

Rule	Description
45CSR60	Control of visible and particulate emissions from stationary sources
45CSR68	Ambient Air Quality Standards
45CSR10	General emission test procedures for sulfur dioxide
45CSR11	Prevention Of Air Pollution Emergency Episodes
45CSR13	Permits-to-Install New Sources and Permit-to-Install and Operate Program
45CSR17	Restrictions of emissions of fugitive dust
45CSR21	Control of emissions of VOCs from stationary sources

1.1.1 Permit Applicability

Air pollution control regulations have been established by the WVDEP for air emissions associated with stationary sources and fugitive emissions resulting from material transfer activities.

To determine permit applicability for the Facility's emission sources, the Potential-to-Emit (PTE) emissions have been presented in Attachment J and Permit Determination Form; the proposed Facility will be considered a minor source with potential uncontrolled PM emissions greater than 25 tons per year (tpy) and less than major source thresholds. Therefore, the Facility will need to obtain a permit to construct and operate. Applicable federal regulations present in Table 1-2 below.

Tetra Tech, Inc. [Application Form](#)

Table 1-2 Federal Applicable Regulations

Rule	Description
40 CFR Part 61 Subpart JJJJ	Standards of Performance for Stationary Spark Ignition Internal Combustion Engines
40 CFR 61 Subpart A	General Provisions
40 CFR 61.18	General control device and work practice requirements

1.1.2 Criteria For Fuel

Processing the plastic fuel stock is not viewed as a waste disposed through incineration, the plastics are being used as a fuel to create a syngas. The process for producing the syngas is through pyrolysis which is classified as an advanced recycling in West Virginia's House Bill 4048.

Terra Tech, Inc. [Application Form](#)

ATTACHMENT E

Plot Plan

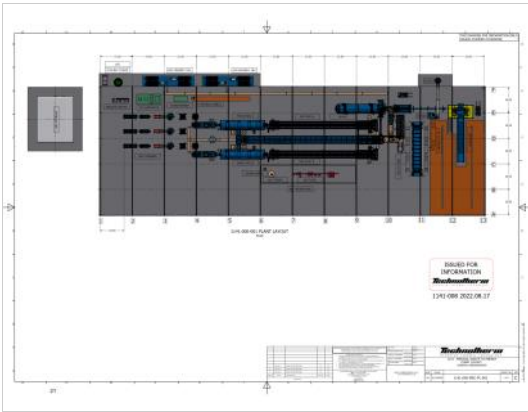
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ATTACHMENT F

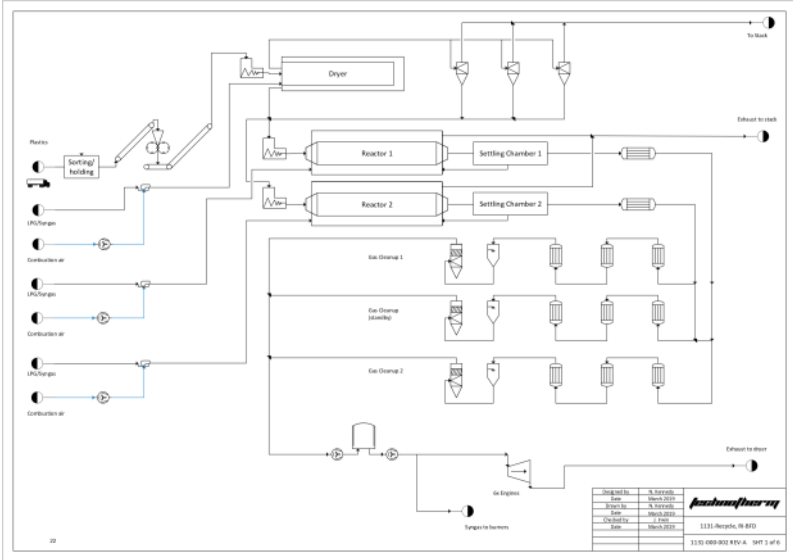
Process Flow Diagram

28



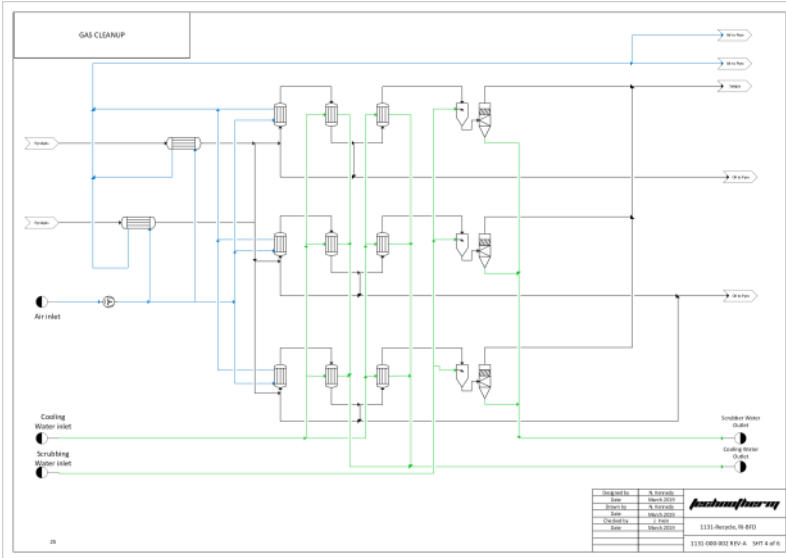
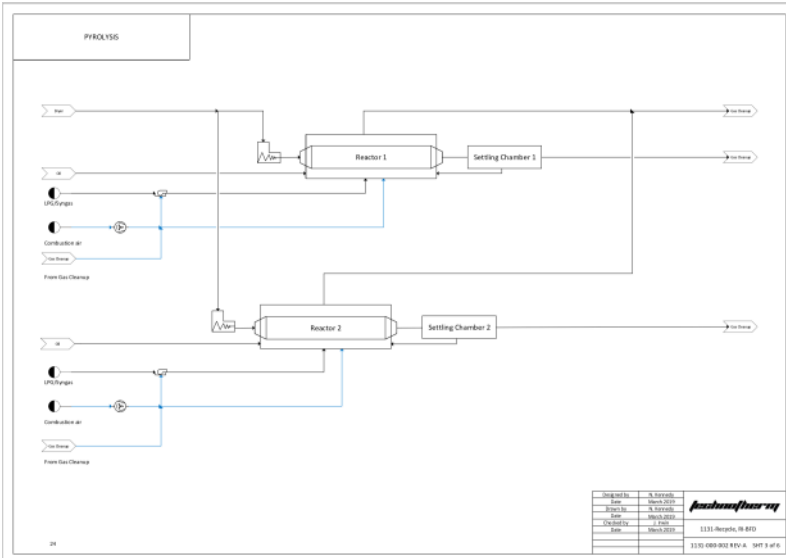
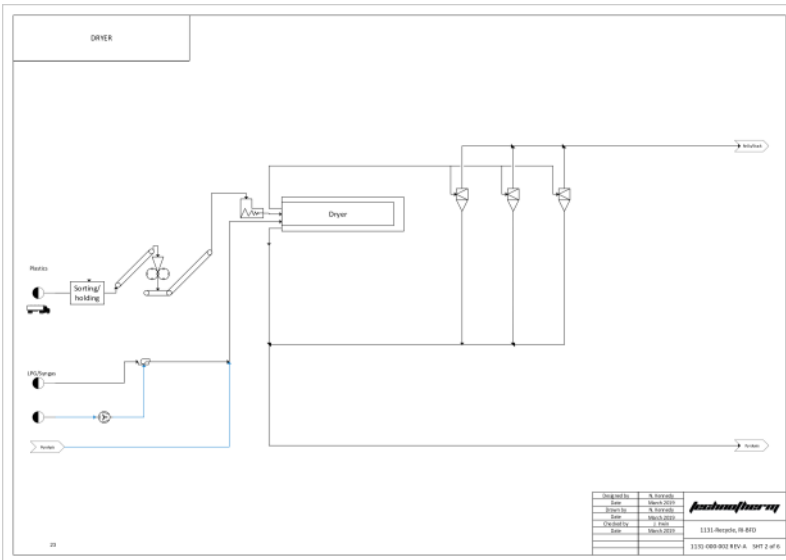
DESIGNED FOR INFORMATION
Rockwell Automation
 1201 000 0022 00 17

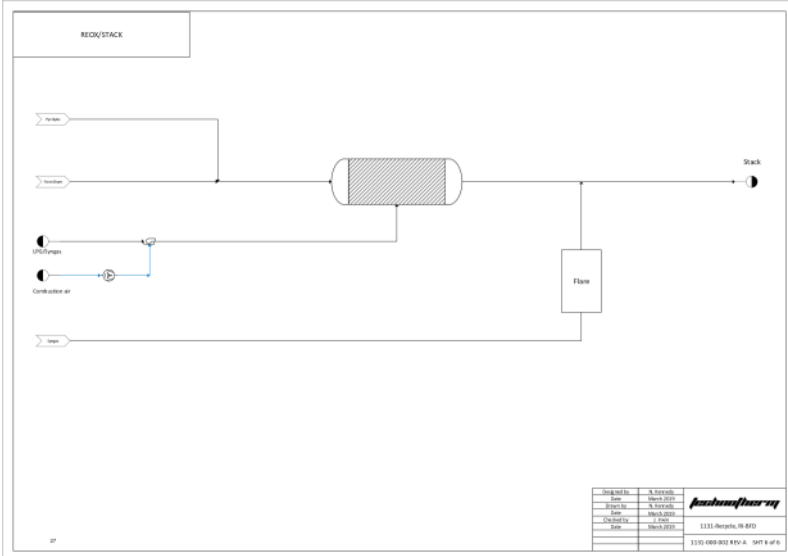
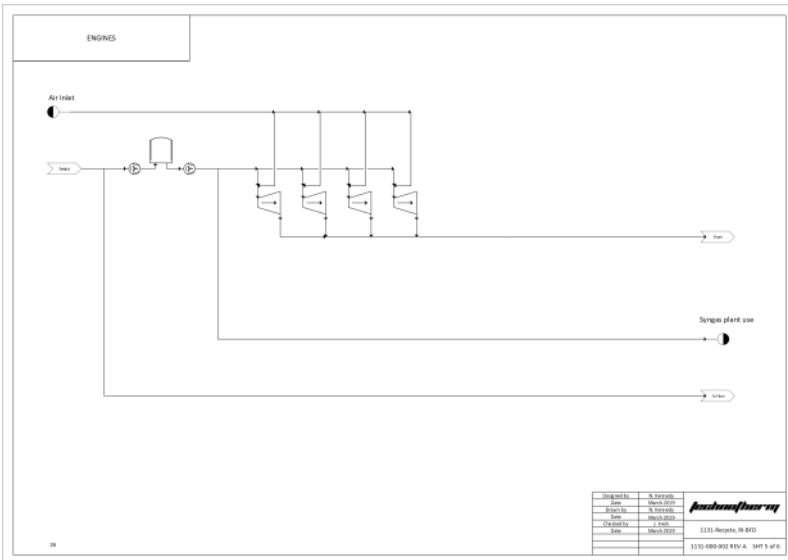
Rockwell Automation
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Date	March 2010	
Design	A. B. B. B. B.	
Design	A. B. B. B. B.	
Date	March 2010	
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Date	March 2010	
		1201 000 0022 00 17
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ATTACHMENT G

Process Description

REQUESTED REVISIONS

- The following revisions from the original permit submital are the following:
- All feedback in new plastic on medical waste will be processed through this system.
 - Clarified value of Fe-Ted stock
 - Plastics will be staged at a separate facility and brought on site as needed.
 - Hydrochloric Acid (HCL) stock loading and associated scrubber system details added.

8. PRE-PROCESSING HANDLING

Feedback will be received from recyclers, manufacturing and plastic producers. Referring to Figure 1, Plastics will be received at an offsite location located in the state of Ohio. The plastics will be sorted by hand and sent to a shredder. The shredder is a developed general generator which will be covered under an Ohio EPA General Air Permit 5-14. The plastics will be shredded to 1" or 4" pieces pieces will then be baled or placed into super sacks and loaded onto trucks for delivery to the facility as needed. The trucks into the site will be controlled by Engine Green Generation and the anticipated truck traffic is to be 400 trucks daily entering into the site via Route 2 from the north.



Figure 1. Flow Diagram for Pre-Processing Handling

2. GENERAL PROCESS DESCRIPTION

Overall process takes plastic, received by a transporting company, and thermally processes it in a pyrolysis system operating at 800°C - 900°C (1,472°F - 2,162°F). Waste composition will consist of plastics with resin particles and through resins. Organic matter and hydrocarbons from the plastics are thermally decomposed without oxygen burning a syngas that can directly be used as a fuel source for emissions generating engines. CO and fuel are produced where the oil is recycled through the pyrolysis system to make more syngas and the tar is used to heat a vibration system in which solids from the process are washed and recycled. The electrical generator's exhausts from the engines are sent to a string unit where the plastic is dried prior to be introduced into the pyrolysis system. All exhaust gases are sent to a Thermal Oxidizer where they are conditioned for release to atmosphere via a stack at a temperature of 850°C (1,562°F).

3. DETAILED PROCESS DESCRIPTION

Referring to Figure 2 below, a detailed description of the process follows where Plastics (P100) is received, sent to Stage 1 (S100) and then to the Macerator (M200), Macerator (M300) operating at 4000 rpm (42.84 Rotations/Min) reduces the Plastics to less than or equal to 20 mm (7/8 inch). Plastics (P100) moves from the Macerator (M200) to the Dryer (D200) and is dried from the exhaust of the fan (F100) (Engine (E100)). Once the Plastics (P100) is dried, it moves to the Feed Silo (S100) through load lock valves. When the Pyrolysis (P200) system is ready to accept feed, load locking valves are actuated such that the feed is put into the Pre-Pyrolysis (P300) system. Condensated water activation is used to keep oxygen level from air below 2.5% in the Pre-Pyrolysis (P300) and Pyrolysis (P400) systems. Chlorides are driven off in the Pre-Pyrolysis (P300) and processed into hydrochloric acid to be sold; also, plastics (P100) is being processed in the Pyrolysis (P400) system, organic matter and hydrocarbons are thermally decomposed forming syngas and moves to the Gas Cleanup (G100). The Gas Cleanup (G100) removes particulate matter and performs the bulk of neutralizing acid forming gases. Next, the gas passes to the Scrubber (S200) where dry acid gases are further removed from the syngas. The syngas then proceeds to the Gasometer (G200) which helps regulate the pressure in the Engine (E200). Syngas is combusted in the Engine (E200) and the exhaust is sent to Dryer (D200). Exhaust from the Dryer is drawn through the Cyclone (C200) and then to the Feed Silo (S200). The Vitrifier (V200) exhaust flows to the Pyrolysis (P400) system, that makes a single pass through the outer chamber of the Pyrolysis (P400) system where additional heat is provided. Next the gases flow through the Dryer (D200). Gases from the Dryer (D200) (exhaust) is sent to the Thermal Oxidizer (TO) (E300) through Cyclone (C200). The (E300) is mixed with Air (A200) and heats the Vitrifier (V200) sufficiently to make a hard solid product (V200) which is ready to be shipped. CO (E300) is continuously recycled through the Pyrolysis (P400) system. Off-gas from the Thermal Oxidizer (E300) are sent through the Stack (S100) which includes an emergency lock, prior to being released into the atmosphere.

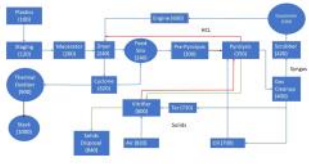


Figure 2. Block flow diagram for detailed process description.

SUB-SYSTEM OPERATION FROM EQUIPMENT DETAIL

Prime Equipment & Systems

The following descriptions supplement the Process Flow Diagrams (PFDs) shown in Figure 1.

1. Delivery of Plastics

The material will be off-loaded from five (5) tractor trailers per day and tipped onto the receiving conveyor with the use of belt tipping systems as shown in Figure 2.



Figure 2. Illustration of typical belt tipping station.

The waste operator will record the weight of each load prior to tipping. Additionally, a weighbridge operator records the weight of the trucks as they enter and exit the plant.

The material will automatically feed the Macerator required and directed by the plant control philosophy.

An air extraction system is built into the Macerator with an extraction fan pulling from the top side of the Macerator at a rate of 1.2 m³/sec. Macerator will be under negative pressure of -0.024 kPa at all times during operation.



Figure 4. Negative Pressure from Macerator to Thermal Oxidizer.
Note all areas prior to thermal oxidation are sealed and under negative pressure.

Further detail, quality grade is prepared sealed containers are delivered to the plant and placed on an input conveyor. After placing on the conveyor operator has no further involvement with the waste.

Material input conveyor

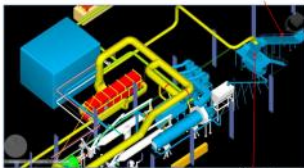


Figure 5.

2. Materials input conveyor to Macerator under negative pressure to Thermal Oxidizer.

The shredder / macerator has a single opening that is sealed, allowing the waste to enter as presented through a single entry point under suction that is closed when waste is not presented for an extended period or during AHA down mode.

The entire facility is closed to the operating environment and operates under a negative pressure (-0.024 kPa), ensuring no escape of odors or pathogens.

Transfer from the Macerator to the dryer and from the dryer to the thermal pre-cyclone is also sealed to the environment operating under a negative pressure.

Progression to the high temperature pyrolysis unit (Fig. 3) is again sealed.

The main fan that is creating a negative pressure is an induced Draft Fan. This fan is connected to the regenerative thermal oxidizer, from the thermal oxidizer to the Macerator, dryer and all material interfaces.



Figure 6. The Regenerative thermal oxidizer is maintained at 850°C.

2.1 Interlocks: The plant cannot be overgrown unless the ID fan is on and the Thermal oxidizer at temperature. There is no possibility of odors.

If the Thermal Oxidizer goes below a predetermined temperature, the plant goes into shut down mode. In the event of a power failure the main control functions are controlled via UPS. In this time a normally closed solenoid valve will have closed the only orifice on the plant which it when the waste is loaded.

In the unlikely event of an ID fan failure (never had one in 25 years) the plant will again default to shut down mode.

2.2 Macerator Degrader Process

Macerator material (feed stock) is conveyed to the Thermal dryer feed hopper. Figure 6 shows a typical Macerator system.



Figure 7. Photos of a typical Macerator/Blender system.

3. Thermal Dryer

The drying of the feed stock is carried out in a direct heated, parallel flow, rotary twin drum type dryer using a combination of engine exhaust and, if necessary, during start-up, or unusual operating conditions, propane and, as a last resort, propane.

Feed stock is transported from the dryer feed hopper into the dryer by means of a screw conveyor. Upon entering the dryer inner shell, the moist feed stock comes into direct contact with the parallel stream of hot

Flue gases

Flues and progression plates ensure intimate contact between the feed stock and flue gas therefore facilitating efficient drying, stabilization and movement of feed stock along the rotator. Once full feed stock and flue gases reach the closed end of the dryer they are discharged from the inner concentric section to the outer shell and return to the entry end of the dryer, discharging 10% moisture feed stock into an expansion silo. Coarse dry feed stock falls to the bottom of the chamber forming a heap on the feed conveyor located beneath.

The flue gas exhaust, concentrated with light particulate feed stock material, is also discharged from the expansion chamber and ducted to a bank of cyclones where separation occurs. Fine particulate dust to the bottom of each cyclone and is discharged via a hopper where it is conveyed to a common conveyor. The coarse material discharges the fine product into the belt conveyor joining the dryer exit material and fine product. This conveyor handles the combined dry feed stock streams into a conveyor leading an intermediate storage hopper that feeds both Pyrolyser.

The cooled flue gas stream from the cyclones is directed to the Thermal

Chiller. 7 and 8 shows photos of a typical dryer in operation.



Figure 8. Photos of a typical dryer in operation from first floor level.



Figure 9. Photos of a typical dryer in operation from ground floor level.

4. Pyrolyser & Ventilation Furnace

Overview

The Pyrolyser takes in feed stock feed stock from a Thermal dryer as described in the previous section. The Pyrolyser train consists of two identical Pyrolysers. The gas, the source of exhaust heat is primarily hot exhaust flue gas from a ventilation furnace located beneath the pyrolyser rotator. These hot flue gases heat the pyrolyser materials and then progress to the medium grade feed application Thermal Dryer and during start up, Propane Cooler and Air Condensers. Supplemental heating of the pyrolyser rotator is being provided by direct injection of the cleaned propane. Natural gas (LPG) is available for initial start up or any shut-down where sufficient propane is available. After passing through the dryers the gas is projected to the Thermal Chiller.

Detailed Description

Feed stock is transferred from the dryer to a live bottom screw hopper, which feed an inlet hopper complete with horizontal material feed screw. Material is fed from a gas-tight, storage hopper into the horizontal, vertically sloped, rotary drum Pyrolyser Rotator by a rotary screw.

As the material passes through the pyrolysis reactor, it undergoes thermal degradation releasing volatile organic oxygen compounds that are discharged from the reactor. The volatile oxygen off-gases are collected into a common manifold that transfers the syngas to the syngas cleaning system.

The heavier particles, mainly comprising of ash and fuel carbon, collect in a specially designed high temperature de-acceleration chamber where the particles are collected and returned to the verification furnace.

The Pyrolyzers must be designed and arranged such that no personnel for harmful situations shall exist under any load condition and shall be complete with all auxiliary equipment for safe, reliable and efficient operation, and for all process design variables of the required continuous, intermittent and transient operation and be suitable for its intended location. The design and materials of construction shall take full into account the location.

Ash and carbonaceous residue produced by the Pyrolyzers drops off the shell from the aforementioned de-acceleration chamber screw conveyor, together with the light residue collected from the base of the Pyrolyzer into a Water, a refractory shell furnace fired by recovered tars (described below in the syngas cleaning equipment). The heat liberated by burning the tars and oils is sufficient to heat the ash from the Pyrolyzer units above their subsiding temperature with moisture, preventing ash to burn off the tars. The char is completely combusted into CO₂ and H₂O.

Figure 10.11 and 2 show photos of Pyrolyzers in operation.



Figure 10. Photo A of typical high temperature pyrolysis unit.



Figure 11. Photo B of typical high temperature pyrolysis unit.



Figure 12. Photo of typical low temperature pyrolysis unit.

5. Syngas Cleanup

Particulate Matter (PM Cleanup)

Raw syngas is removed from the Pyrolysis Reactors, as described above, and passes through a de-acceleration chamber and then hot cyclones. The cyclones are arranged for parallel flow to ensure maximum PM removal efficiency during start-up and shutdown as the flow varies. PM drops to specially designed hot screw conveyors and from there is directed to the verification/furnace described above.

Syngas Coolers

The partially cleaned, still hot, raw gas flows next through stainless steel tubular syngas coolers. The cooler is in essence a Heat Exchanger which indirectly transfers heat from syngas to the combustion air heaters.

Tar Condensers

The syngas from the coolers described above flows to a stainless-steel shell & tube Heat Exchanger cooler that is cooled by an air blower system. Tars are condensed out and drop into heated troughs, the heat source of which is engine exhaust that is conditioned for its transport to the verification furnace described above. The condensed material opens off coolers into engine exhaust troughs to heat the heat exchangers and thereby cause the tars to drop into the heated trough below.

Oil Coolers

The syngas from the tar condensers described above flows to a shell & tube Heat Exchanger/cooler that are cooled by water cooling system. Condensed oils, which also contain condensed water, are collected and is pumped to the vitrification furnace described previously. The common installed square unit of condenser uses engine exhaust fan gas to heat the heat exchanger and thereby cause the oils to drop into the heated trough below.

Vertical Scrubbers

From the oil condensers the syngas flows through a high pressure drop Vertical Scrubber to remove any remaining PM.

Figure 13 and 14 show photos of a typical gas cleanup system in operation.



Figure 13. Photo A of a typical gas cleanup system in operation.



Figure 14. Photo B of a typical gas cleanup system in operation.

Gas Bladder (Syngas Storage Tank)

The syngas storage tank provides surge capacity of cleaned syngas to level out flow and composition variations. It shall be a bladder contained within a dewatered area. The bladder will operate with an internal pressure of 30 to 40 millibar gauge.

Figure 15 shows a typical gas bladder in operation.



Figure 15. Picture of typical gas bladder.

Stack

The hot gases progress through the stack in to the atmosphere after passing through the Thermal Oxidizer (discussed in next section).

6. Thermal Oxidizer

After passing through a scrubber the flue gases enter a Thermal Oxidizer consisting of a rectangular box shaped furnace. The internal dimensions are determined by the total volume that needs to be raised to 850 °C and maintained for 2 seconds.

Figure 16 shows a typical Thermal Oxidizer in operation. Please refer to the technical specification file for more details if required.



Figure 16 Photo of a typical Thermal Oxidizer in operation.

7. Syngas Engines

Each syngas engine shall be a fully packaged unit complete with all associated components and auxiliaries. These engines are of robust design and have been proven on low and medium capacity value gas fuels.

The engine package will be complete to allow the engine to start, synchronize, operate continuously at base or part load and shut down.

The syngas engines shall be assembled in containers as indicated on the plant layout. The containerized engines shall conform to a sound pressure level of 80 dBA (2005 Noise Regulations off-action level) as measured one meter from the enclosure at no-load close door level.

Notwithstanding the syngas start-up equipment and systems described in the Syngas Clean up Section above, the syngas engine exhaust systems shall be designed and installed such that they meet emissions standards as of the Commissioned Date.

The Engine cooling will be by means of external radiators; they shall be designed and constructed with sufficient margin and spare surface area for the maximum heat rejection duty under all operating conditions.

The radiators shall incorporate features to minimize corrosion and erosion on the air and water side and suitable provisions for cleaning and core replacement.

The radiators and all of their component parts shall be of proven design and arranged so as to minimize maintenance work.

Figure 17 and Figure 18 illustrate the containerized engines in production.

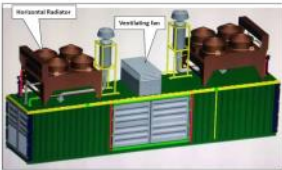


Figure 17. Illustration A of containerized engines in production.

ATTACHMENT H

**Material Data Safety Sheets (MSDSs)
Safety Data Sheets (SDSs)**

**Section 1: Identification****Product Identifier****Product Name** - Synthetic Natural Gas**Relevant identified uses of the substance or mixture or mixture and uses advised against****Recommended use** - Fuel for combustion applications, see material for chemical reactions**Details of the supplier of the safety data sheet****Manufacturer**
- Dakota Gasification
420 County Road 26
Beulah, WY 82401-9430
United States
www.dakotagas.com**Telephone (General)** - 701-873-2100**Emergency Contact Information****Email** - SDS@emerge@dgpc.com
Manufacturer - 701-873-6900
CHEMTREK - 800-424-9300**Section 2: Hazard Identification****United States (US)**According to **CGHA 26 CFR 1910.1200 HCS****Classification of the substance or mixture****CGHA HCS 2012**
- Flammable Gases - H220
- Compressed Gas - H280
- Simple Asphyxiant**Label elements****CGHA HCS 2012****Hazard statements** - Extremely flammable gas - H220
Contains gas under pressure, may explode if heated - H280
May displace oxygen and cause rapid asphyxiation.**Product Name:** Synthetic Natural Gas
Revision Date: 10/02/2019

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Precautionary statements**Prevention** - Keep away from heat, sparks, open flames and/or hot surfaces. - No smoking. - P210
Response - Leaking gas fire: Do not extinguish, unless safe can be stopped safely. - P277
Eliminate all ignition sources if safe to do so. - P501**Storage/Disposal** - Protect from sunlight. Store in a well-ventilated place. - P410+P403**Other hazards****CGHA HCS 2012**
- Under United States Regulations (29 CFR 1910.1200 - Hazard Communication Standard),
the product is considered hazardous.**Canada**According to **WHMIS****Classification of the substance or mixture****WHMIS** - Compressed Gas - A,
Flammable Gases - B1**Label elements****WHMIS**- Compressed Gas - A
Flammable Gases - B1**Other hazards****WHMIS** - This material is a simple asphyxiant. May displace or reduce oxygen available for breathing especially in confined spaces.
In Canada, the product mentioned above is considered hazardous under the Workplace Hazardous Materials Information System (WHMIS).**Section 3: Composition information on ingredients****Substances**

- Material does not meet the criteria of a substance.

Mixtures

Composition					
Chemical Name	Identifiers	%	LOEL/LOAEL	Classification According to Regulatory/Trade	Comments
Methane	CAS:75-08-0	95%	N/A	CGHA HCS 2012: Flam. Gas 1, Press. Gas - Comp., Tox., Irritant	N/A

Product Name: Synthetic Natural Gas**Revision Date:** 10/02/2019

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Hydrogen	CAS:1333-74-0	3.1%	N/A	CGHA HCS 2012: Flam. Gas 1, Press. Gas - Comp., Tox., Irritant	N/A
Carbon Dioxide	CAS:7440-44-0	1.1%	Irritation: Eye (OECD) - XN; Irritation: Skin (OECD) - XN; Irritation: Respiratory (OECD) - XN	CGHA HCS 2012: Press. Gas - Comp., Simple Asphyxiant	N/A

Section 4: First-Aid Measures**Description of first aid measures****Inhalation** - If INHALED: Remove victim to fresh air and keep at rest in a position comfortable for breathing. Administer oxygen if breathing is difficult. Give artificial respiration if victim is not breathing. If signs/symptoms continue, get medical attention.**Skin** - If ON SKIN: Wash with plenty of soap and water. If skin irritation occurs, get medical advice/attention. Wash contaminated clothing before reuse.**Eye** - If IN EYES: Flush cautiously with water for several minutes. Remove contact lenses, if present and easy to do. Continue rinsing. If eye irritation persists, get medical advice/attention.**Ingestion** - Ingestion is not anticipated to be a likely mode of exposure to this product.**Most important symptoms and effects, both acute and delayed**

- Refer to Section 11 - Toxicological Information.

Indication of any immediate medical attention and special treatment needed**Notes to Physician** - All treatments should be based on observed signs and symptoms of distress in the patient.

Consideration should be given to the possibility that overexposure to materials other than this product may have occurred.

Other information

- Ensure that medical personnel are aware of the material(s) involved and take precautions to protect themselves. RESCUERS SHOULD NOT ATTEMPT TO RETRIEVE VICTIMS OF EXPOSURE TO GASES WITHOUT APPROPRIATE PERSONAL PROTECTIVE EQUIPMENT. As a minimum, Self-Contained Breathing Apparatus must be worn. Victims who experience any adverse effect after over-exposure to this gas mixture must be taken for medical attention. Rescuers should be taken for medical attention if necessary. Take a copy of the label and the MSDS to physician or other health professional with victims.

Section 5: Fire-Fighting Measures**Extinguishing media****Substance Extinguishing Media** - SMALL FIRES: Dry chemical or CO2.
Media - LARGE FIRES: Water spray or fog.**Unsuitable Extinguishing Media** - No data available.**Special hazards arising from the substance or mixture****Unstable Fire and Explosion Hazards** - EXTREMELY FLAMMABLE. Will form explosive mixtures with air.

- Vapors may travel to source of ignition and flash back.

- Cylinders exposed to fire may vent and release flammable gas through pressure relief devices.

- Containers may explode when heated.

- Ruptured cylinders may leak.

Product Name: Synthetic Natural Gas**Revision Date:** 10/02/2019

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Burns with a pale, fairly luminous flame, or containing more than 14% methane burn without noise.

Hazardous Combustion • No data available

Products

Advice for firefighters

- Structural firefighters protective clothing provides limited protection in fire situations ONLY. It is not effective in self-sustaining fires where direct contact with the substance is possible.
- Wear positive pressure self-contained breathing apparatus (SCBA).
- DO NOT EXTINGUISH A LEAKING GAS FIRE UNLESS LEAK CAN BE STOPPED.
- Most containers from the area if you can do it without risk.
- FIRE: If tank, rail car or tank truck is involved in a fire, ISOLATE for 100 meters (1 mile) in all directions; also consider initial evacuation for 100 meters (1 mile) in all directions.
- FIRE INVOLVING TANKS: ALWAYS stay away from tanks engulfed in fire.
- FIRE INVOLVING TANKS: Fight fire from maximum distance or use unmanned hose holders or monitor nozzles.
- FIRE INVOLVING TANKS: Withdraw immediately in case of rising sound from venting safety devices or discoloration of tank.
- FIRE INVOLVING TANKS: Cool containers with flooding quantities of water until well after fire is out.
- FIRE INVOLVING TANKS: Do not direct water at source of leak or safety devices, long pipe nozzle.
- FIRE INVOLVING TANKS: For maximum fire, use unmanned hose holders or monitor nozzles. If this is impossible, withdraw from area and let fire burn.

Section 6 - Accidental Release Measures

Personal precautions, protective equipment and emergency procedures

Personal Precautions • Do not touch damaged containers or spilled material unless wearing appropriate protective clothing. Do not walk through spilled material. Ventilate the area before entry.

Emergency Procedures • ELIMINATE all ignition sources (no smoking, flames, sparks or flames in immediate area). As an immediate precautionary measure, isolate spill or leak area for at least 100 meters (100 feet) in all directions. Stop work if you can do it without risk. Keep unauthorized personnel away. Keep out of low areas. Stay upwind. LARGE SPILL: Consider initial downwind evacuation for at least 100 meters (1/2 mile) if spilled material is encountered which cannot be stopped by shutting off the closed appropriate valve or main supply valve (without risk). Evacuate a zone for evacuation and quickly contact the local fire department.

Environmental precautions

• Prevent spreading of vapors through screens, ventilation systems and confined areas.

Methods and material for containment and cleaning up

Containment/Clean-up • All equipment used when handling the product must be grounded. Stop work if you can do it without risk. If possible, turn leaking containers so that gas escapes rather than liquid. Use water spray to reduce vapors, direct and put water directly on tank, spill area or inside container. Do not direct water at spill or source of leak, before area until gas has dispersed.

Section 7 - Handling and Storage

Product Name: Synthetic Natural Gas
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Precautions for safe handling

Handling • Keep away from heat and ignition sources - No Smoking. Take precautionary measures against static charges. All equipment used when handling the product must be grounded. Use only non-sparking tools. Use only well-ventilated areas. Ventilate closed spaces before entering. Be aware of any signs of dizziness or fatigue, especially if work is done in a poorly ventilated area. Exposure to high concentrations of this gas mixture could occur without any significant warning symptoms, due to efficiency failure or oxygen deficiency. Cylinders should be firmly secured to prevent falling or being knocked-over. Use explosion-proof electrical, ventilating and lighting equipment. Do not attempt to repair, weld, or any other way modify cylinders. If there is a malfunction or another type of operational problem, contact nearest distributor immediately. Empty containers retain product residue and can be hazardous. Do not cut, weld, puncture or incinerate container.

Conditions for safe storage, including any incompatibilities

Storage • Cylinders should be stored in dry, well-ventilated areas away from sources of heat, ignition and direct sunlight. Do not allow areas where cylinders are stored to exceed 50°C (125°F). Cylinders must be protected from the environment, and preferably kept at room temperature approximately 21°C (70°F). Protect cylinders against physical damage. Cylinders should be firmly secured to prevent falling or being knocked-over. Store locked up.

Section 8 - Exposure Controls/Personal Protection

Control parameters

Exposure Limits/ Guidelines	ACGIH		NIOSH		OSHA
	TLV	STEL	TLV	STEL	
Asphyxiant (C ₂ H ₆)	1000 ppm TWA	1000 ppm STEL	1000 ppm TWA; 1000 ppm STEL	1000 ppm STEL	1000 ppm TWA; 1000 ppm STEL
Methane (CH ₄)	100 ppm TWA (short-term exposure limit)	Not established	Not established	Not established	Not established

Exposure controls

Engineering Measures/Controls • Good general ventilation should be used. Ventilation rates should be matched to conditions. If applicable, use process enclosures, local exhaust ventilation, or other engineering controls to maintain airborne levels below recommended exposure limits. If exposure limits have not been established, maintain airborne levels to an acceptable level. Use explosion-proof electrical, ventilating and lighting equipment.

Personal Protective Equipment

Respiratory • Follow the OSHA respirator regulations found in 29 CFR 1910.134. Use an NIOSH/MSHA approved respirator if exposure limits are exceeded or symptoms are experienced.

Eye/Face • Wear safety glasses.

Hand/body • Wear rubber gloves when handling cylinders.

Environmental • Follow local practices for site management and disposal of waste. Controls should be engineered to prevent release to the environment, including procedures to prevent spills, atmospheric release and release to wastewater.

Key to abbreviations
ACGIH: American Conference of Governmental Industrial Hygienists
NIOSH: National Institute of Occupational Safety and Health
OSHA: Occupational Safety and Health Administration
STEL: Short-Term Exposure Limit as based on 15-minute exposure
TWA: Time-Weighted Average as based on 8-hour, 40-hour exposure

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Section 9 - Physical and Chemical Properties

Information on Physical and Chemical Properties

Physical Description	Color	Appearance/Description	Odorless gas with a HSE label
Physical Form	Gas		
Color	Colorless		
Odor	Odorless		
General Properties			
Density	0.717 g/L @ 15°C	Relative Density	0.554 (air = 1.000)
Boiling Point	-162°C (-260°F)	Freezing Point	-182°C (-288°F)
Specific Gravity (Relative Density)	0.554 (air = 1.000)	Sublimation	Not applicable
Water Solubility	Highly Soluble	Flammability	Not applicable
Common Properties	Not applicable	Reactivity	Not applicable
Volatility			
Vapor Pressure	Not applicable	Vapor Density	0.554 (air = 1.000)
Evaporation Rate	Not applicable	Evaporation Rate (1)	0.001
Flammability			
Flash Point	Not applicable	LEL	5% (v/v)
UFL	Not applicable	Sublimation	Not applicable
Flammability (in air)	Flammable Gas		
Environmental			
Biodegradability (in air)	Not applicable		

Section 10: Stability and Reactivity

Reactivity

• No hazardous reaction known under conditions of normal use.

Chemical stability

• Stable

Possibility of hazardous reactions

• Hazardous polymerization will not occur.

Conditions to avoid

• Incompatible materials: Avoid contact with heat and ignition sources. Excess heat.

Incompatible materials

• Reacts violently with powerful oxidizers (e.g. bromine pentafluoride, chlorine trifluoride, chlorine, fluorine, dioxane, nitrogen trichloride, nitrogen tetroxide, nitrogen dioxide, nitrogen difluoride, nitrogen dioxide, liquid oxygen).

Hazardous decomposition products

• No data available.

Section 11 - Toxicological Information

Information on toxicological effects

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Compartments	
Reserve (50%)	75L 2.0L
Carbon dioxide (17%)	124 3.0

OSHA Hierarchy	Classification
Acute toxicity	OSHA HCS 2012 (Cite testing)
Respiratory hazard	OSHA HCS 2012 (Cite testing)
Flammability	OSHA HCS 2012 (Cite testing)
Corrosion/irritation	OSHA HCS 2012 (Cite testing)
Health hazard	OSHA HCS 2012 (Cite testing)
Physical hazard	OSHA HCS 2012 (Cite testing)
OSHA 68	OSHA HCS 2012 (Cite testing)
OSHA 69	OSHA HCS 2012 (Cite testing)
OSHA 70	OSHA HCS 2012 (Cite testing)
OSHA 71	OSHA HCS 2012 (Cite testing)
OSHA 72	OSHA HCS 2012 (Cite testing)
OSHA 73	OSHA HCS 2012 (Cite testing)
OSHA 74	OSHA HCS 2012 (Cite testing)
OSHA 75	OSHA HCS 2012 (Cite testing)
OSHA 76	OSHA HCS 2012 (Cite testing)
OSHA 77	OSHA HCS 2012 (Cite testing)
OSHA 78	OSHA HCS 2012 (Cite testing)
OSHA 79	OSHA HCS 2012 (Cite testing)
OSHA 80	OSHA HCS 2012 (Cite testing)
OSHA 81	OSHA HCS 2012 (Cite testing)
OSHA 82	OSHA HCS 2012 (Cite testing)
OSHA 83	OSHA HCS 2012 (Cite testing)
OSHA 84	OSHA HCS 2012 (Cite testing)
OSHA 85	OSHA HCS 2012 (Cite testing)
OSHA 86	OSHA HCS 2012 (Cite testing)
OSHA 87	OSHA HCS 2012 (Cite testing)
OSHA 88	OSHA HCS 2012 (Cite testing)
OSHA 89	OSHA HCS 2012 (Cite testing)
OSHA 90	OSHA HCS 2012 (Cite testing)
OSHA 91	OSHA HCS 2012 (Cite testing)
OSHA 92	OSHA HCS 2012 (Cite testing)
OSHA 93	OSHA HCS 2012 (Cite testing)
OSHA 94	OSHA HCS 2012 (Cite testing)
OSHA 95	OSHA HCS 2012 (Cite testing)
OSHA 96	OSHA HCS 2012 (Cite testing)
OSHA 97	OSHA HCS 2012 (Cite testing)
OSHA 98	OSHA HCS 2012 (Cite testing)
OSHA 99	OSHA HCS 2012 (Cite testing)
OSHA 100	OSHA HCS 2012 (Cite testing)

Potential Health Effects

Inhalation

Acute (Immediate) • This material is a simple asphyxiant. May displace or reduce oxygen available for breathing especially in confined spaces. If this material is released in a small, poorly ventilated area (i.e. an enclosed or confined space), an oxygen deficient environment may occur. Individuals breathing such an atmosphere may experience symptoms which include headache, dizziness, nausea, vomiting, loss of consciousness, unconsciousness, respiratory collapse and death. Under some circumstances of over-exposure, death may occur. The following effects associated with decreased levels of oxygen: increase in breathing and pulse rate, emotional upset, abnormal fatigue, nausea, vomiting, collapse, loss of consciousness, convulsive movements, respiratory collapse and death.

Chronic (Delayed) • No data available

Skin (Immediate) • Under normal conditions of use, no health effects are expected.

Chronic (Delayed) • No data available

EYE (Immediate) • Under normal conditions of use, no health effects are expected.

Chronic (Delayed) • No data available

Ingestion

Acute (Immediate) • Under normal conditions of use, no health effects are expected.

Chronic (Delayed) • No data available

Key to abbreviations
LC = Lethal Concentration
TL = Test Concentration

Section 12 - Ecological Information

Toxicity

• Material data lacking

Persistence and degradability

• Material data lacking

Bioaccumulative potential

• Material data lacking

Mobility in Soil

• Material data lacking

Results of PBT and vPvB assessment

• PBT and vPvB assessment has not been conducted for this material.

Other adverse effects

• No studies have been found.

Section 13 - Disposal Considerations

Waste treatment methods

Product waste • Dispose of content and/or container in accordance with local, regional, national, and/or international regulations.

Packaging waste • Dispose of content and/or container in accordance with local, regional, national, and/or international regulations.

Section 14 - Transport Information

UN number	UN proper shipping name	Transport hazard class(es)	Packing group	Environmental hazards
DOT UN1950	Compressed gas, flammable, toxic (Methane and Hydrogen)	2.1	NEA	NEA
TDB UN1950	Compressed Gas - Liquefiable, N.O. 2.1 (Methane and Hydrogen)	2.1	NEA	Flammable (Gases), Toxic (Gases)
MSDASD UN1950	Compressed gas, flammable, toxic (Methane and Hydrogen)	2.1	NEA	NEA

Special precautions for user • Cylinders should be transported in a secure position, in a well-ventilated vehicle. The transportation of compressed gas cylinders in automobiles or in closed-body vehicles

compartments unless safety hazards. If transporting these cylinders in vehicles, ensure these cylinders are not exposed to extremely high temperatures (as may occur in an enclosed vehicle on a hot day). Additionally, the vehicle should be well-ventilated during transportation.

Transport to bulk according to Annex B of MARPOL 73/78 and the IBC Code

• No data available

Section 15 - Regulatory Information

Safety, health and environmental regulations/legislation specific for the substance or mixture

SARA Hazard Classifications • Acute: F (Toxic), Pressure (Gases/Release of)

Component	CAS	Canada DSL	Canada NDSL	EU F/NECS	EU F/NECS	Keene ECEL
Carbon dioxide	124-38-2	Yes	No	Yes	No	Yes
Hydrogen	1333-74-0	Yes	No	Yes	No	Yes
Methane	74-82-6	Yes	No	Yes	No	Yes

Canada

Labels

Canada - WHMIS - Classifications of Substances

-Hydrogen	1333-74-0	A, B1
-Carbon dioxide	124-38-2	A, Uncontrolled product according to WHMIS classification (toxic gases)
-Methane	74-82-6	A, B1

Canada - WHMIS - Ingredient Disclosure List

-Hydrogen	1333-74-0	Not Listed
-Carbon dioxide	124-38-2	1%
-Methane	74-82-6	Not Listed

Environmental

Canada - CEPA - Priority Substances List

-Hydrogen	1333-74-0	Not Listed
-Carbon dioxide	124-38-2	Not Listed
-Methane	74-82-6	Not Listed

United States

Labels

U.S. - OSHA - Process Safety Management - Highly Hazardous Chemicals

-Hydrogen	1333-74-0	Not Listed
-Carbon dioxide	124-38-2	Not Listed
-Methane	74-82-6	Not Listed

U.S. - OSHA - Specifically Regulated Chemicals

-Hydrogen	1333-74-0	Not Listed
-Carbon dioxide	124-38-2	Not Listed
-Methane	74-82-6	Not Listed

Environmental

U.S. - CAA (Clean Air Act) - 1990 Hazardous Air Pollutants

-Hydrogen	1333-74-0	Not Listed
-Carbon dioxide	124-38-2	Not Listed

Methane	74.824	Not Listed
U.S. - OSHA/MSHA - Hazardous Substances and their Reportable Quantities		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed
U.S. - OSHA/MSHA - Reportable and Their Reportable Quantities		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed
U.S. - OSHA/MSHA - Section 302 Extremely Hazardous Substances EPCRA RQs		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed
U.S. - OSHA/MSHA - Section 302 Extremely Hazardous Substances TPGs		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed
U.S. - OSHA/MSHA - Section 303 - Release Reporting		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed
U.S. - OSHA/MSHA - Section 303 - P81 Chemical Listing		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed
Inventory - United States - Section 303 Inventory (TSCA) - P81 Number to EPA Accession Number List		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed

United States - California		
Environmental		
U.S. - California - Proposition 65 - Carcinogens List		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed
U.S. - California - Proposition 65 - Developmental Toxicity		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed
U.S. - California - Proposition 65 - Maximum Allowable Dose Levels (MADL)		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed
U.S. - California - Proposition 65 - No Significant Risk Levels (NSRL)		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed
U.S. - California - Proposition 65 - Reproductive Toxicity - Female		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed
U.S. - California - Proposition 65 - Reproductive Toxicity - Male		
Hydrogen	1333.74.0	Not Listed
Carbon dioxide	101.06.9	Not Listed
Methane	74.824	Not Listed

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Section 16 - Other Information

Last Revision Date • 02/03/2019
Preparation Date • 01/03/2014

Key to abbreviations
N/A = Not available

Disclaimer/Statement of Liability

The information contained in this Safety Data Sheet (SDS) is believed to be correct since it was obtained from sources we believe are reliable. However, no representation, guarantee or warranty of any kind is made as to the accuracy, suitability for particular applications, hazards connected with the use of the material, or the results to be obtained from the use thereof. User assumes all risks and liability of any use, processing or handling of any material, variations in methods, conditions and equipment used to store, handle or process the material and hazards connected with the use of the material are solely the responsibility of the user and remain at his sole discretion. Compliance with all applicable federal, state, and local laws and regulations remains the responsibility of the user, and the user has the responsibility to provide a safe work place to ensure all aspects of its operation and to observe it or where provisions, in addition to those described herein, are required.

Product Name: Synthetic Natural Gas Page 11 of 12
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Safety Data Sheet
Material Name: Propane - UN1975 Specific SDS ID: 90246011

Section 1 - PRODUCT AND COMPANY IDENTIFICATION

Material Name: Propane - UN1975 Specific
Synonyms: DIMETHYL HYDROCARBON; PROPANE; DIMETHYL METHANE; PROPANE; HYDROGEN; DIMETHYL HYDROCARBON; LIQUEFIED PETERLEUM GAS (LPG) - 99% NATURAL GRADE - 99% PURE GRADE; C3 H8 C3H8
Chemical Family: Hydrocarbons, aliphatic
Product Description: Classification determined in accordance with Compressed Gas Association standards.
Product Use: Industrial and Specialty Gas Applications.
Restrictions on Use: None known.
Details of the supplier of the safety data sheet: MATHESON TECHNOLOGIES, INC. 801 Lake Canyon Parkway Suite 1000 Irving, TX 75039 General Tel: (972) 441-4100 Emergency Tel: 1-800-441-4100 (U.S. & Canada) Outside the U.S.: 361-527-1867 (U.K. & Ireland)

Section 2 - HAZARDS IDENTIFICATION

Classification in accordance with paragraph 2.1 of GHS 09/13/16:
Flammable Gas - Category 1
Gases Under Pressure - Liquefied gas
Simple Asphyxiant
GHS Label Elements
Signal Word
Hazard Statement
Precautionary Statement
GHS Label Elements



Signal Word: Danger
Hazard Statement: H280: Extremely flammable gas.
Precautionary Statement: P201+P202: Read the label and instructions carefully. P231+P232: Keep away from heat/sparks/open flames/hot surfaces - No smoking.
Precautionary Statement: P231+P232: Keep away from heat/sparks/open flames/hot surfaces - No smoking.
Precautionary Statement: P231+P232: Keep away from heat/sparks/open flames/hot surfaces - No smoking.

Safety Data Sheet

SDS ID: 3024018

Material Name: Propane – UN1059 Specific

UN1059 Specific

ACGIH - Threshold Limit Values - Biological Exposure Indices (BIEI)

There are no biological limit values for any of this product's components.

Engineering Controls

Ventilation equipment should be explosion resistant if explosive concentrations of material are present. Provide local exhaust ventilation systems. Follow compliance with applicable exposure limits. Use check, leak prevention device or drip tray.

Individual Protection Measures, such as Personal Protective Equipment

Respirator protection
For the gas: Eye protection not required, but recommended. For the liquid: Wear splash resistant safety goggles. Contact lenses should not be worn. Provide an emergency eye wash fountain and quick drench shower at the immediate work area.

Skin Protection
For the gas: Protective clothing is not required. For the liquid: Wear appropriate protective, cold insulating clothing.

Respiratory Protection
The following respiratory and maximum use concentrations are drawn from NFPA801 and/or OSHA 29 CFR. Any supplied respiratory equipment must be certified for use with this gas. Emergency or planned entry into unknown concentrations of H2S conditions - Any self-contained breathing apparatus that has a full facepiece and is operated in a pressure-demand or other positive-pressure mode. Any supplied air respiratory with a full facepiece that is operated in a pressure-demand or other positive-pressure mode in combination with an auxiliary self-contained breathing apparatus operated in pressure-demand or other positive-pressure mode. Escape - Any appropriate escape-type, self-contained breathing apparatus.

Chemical Reactivities
Wear resistant gloves.

Section 9 - PHYSICAL AND CHEMICAL PROPERTIES

Property	Value	Physical State	Value
Appearance	colorless gas	Physical State	gas
Odor	gasoline odor	Color	colorless
Odor Threshold	5000-20000 ppm	pH	Not available
Melting Point	-180 °C (-330 °F)	Boiling Point	-42 °C (-44 °F)
Boiling Point Range	Not available	Freezing point	Not available
Evaporation Rate	Not available	Flammability (LFL, UEL)	Flammable gas
Autoignition Temperature	450 °C (842 °F)	Flash Point	-185 °C (-303 °F)
Lower Explosive Limit	2.1 %	Decomposition temperature	Not available
Upper Explosive Limit	9.5 %	Vapor Pressure	0.585 mmHg @ 21.1 °C
Vapor Density (air=1)	1.55	Specific Gravity (water=1)	0.5035 at -45 °C

Safety Data Sheet	
according to 28CFR16101230 and GHS Rev. 3	
Effective date: 01.08.2015	Page 9 of 8
Hydrochloric Acid,ACS	
Reproductive Toxicity	No additional information.
SECTION 12 : Ecological information	
<p>Ecotoxicity</p> <p>7647-01-0 Toxicity to fish LC50: Garibaldi affinis (Masquefin fish): 202 mg/l 96 h Hydrochloric acid</p> <p>Persistence and degradability</p> <p>Biodegradative potential:</p> <p>Stability in soil:</p> <p>Other adverse effects:</p>	
SECTION 13 : Disposal considerations	
<p>Waste disposal recommendations:</p> <p>Do not allow product to reach sewage system or open water. It is the responsibility of the waste generator to properly characterize all waste materials according to applicable regulatory entities (28CFR16101230). Contact a licensed professional waste disposal service to dispose of this material. Dispose of empty containers as a used product. Product or containers must not be disposed together with household garbage. Chemical waste generators must determine whether a discarded chemical is classified as a hazardous waste. Chemical waste generators must also consult local, regional, and national hazardous waste regulations. Consult competent and accurate classification.</p>	
SECTION 14 : Transport information	
<p>UN Number:</p> <p>2708</p> <p>UN proper shipping name:</p> <p>HYDROCHLORIC ACID</p> <p>Transport hazard class(es):</p> <p>Class 8 Corrosive substances</p> <p>Packing group I:</p> <p>Environmental hazard:</p> <p>Transport in bulk:</p> <p>Special precautions for user:</p>	
SECTION 15 : Regulatory information	
<p>United States (USA)</p> <p>SARA Section 311/312 (Specific toxic chemical listings):</p> <p>Acid</p> <p>SARA Section 313 (Specific toxic chemical listings):</p> <p>7647-01-0 Hydrochloric Acid</p> <p>RCRA Hazardous waste code(s):</p> <p>None of the ingredients is listed.</p> <p>TSCA (Toxic Substances Control Act):</p> <p>All ingredients are listed.</p>	

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Safety Data Sheet	
according to 28CFR16101230 and GHS Rev. 3	
Effective date: 01.08.2015	Page 7 of 8
Hydrochloric Acid,ACS	
<p>CEPCLA (Comprehensive Environmental Response, Compensation, and Liability Act):</p> <p>7647-01-0 Hydrochloric Acid 5000 lb.</p>	
<p>Proposition 65 (California):</p> <p>Chemicals known to cause cancer:</p> <p>None of the ingredients is listed.</p> <p>Chemicals known to cause reproductive toxicity for females:</p> <p>None of the ingredients is listed.</p> <p>Chemicals known to cause reproductive toxicity for males:</p> <p>None of the ingredients is listed.</p> <p>Chemicals known to cause developmental toxicity:</p> <p>None of the ingredients is listed.</p>	
<p>Canada</p> <p>Canadian Domestic Substances List (DSL):</p> <p>All ingredients are listed.</p> <p>Canadian WHMIS Ingredient Disclosure List (Block 1, 1%):</p> <p>None of the ingredients is listed.</p> <p>Canadian WHMIS Ingredient Disclosure List (Block 2%):</p> <p>7647-01-0 Hydrochloric Acid</p>	
SECTION 16 : Other information	
<p>The product has been classified in accordance with hazard criteria of the Controlled Products Regulations and the SDS contains all the information required by the Controlled Products Regulations. Note: The responsibility to provide a safe workplace remains with the user. The user should consider the health hazards and safety information contained herein as a guide and should take those precautions required in an industrial operation to reduce employees and blowing work practice procedures for a safe work environment. The information contained herein is to the best of our knowledge and belief, accurate; however, under the conditions of handling and use are beyond our control, we make no guarantee of results, and assume no liability for damages incurred by the use of this material. It is the responsibility of the user to comply with all applicable laws and regulations applicable to this material.</p> <p>GHS Full Text Phrases:</p> <p>Abbreviations and acronyms:</p> <p>IMDG: International Maritime Code for Dangerous Goods PEL: Permissible Exposure Concentration (NIOSH) CFR: Code of Federal Regulations (USA) SARA: Superfund Amendments and Reauthorization Act (USA) RCRA: Resource Conservation and Recovery Act (USA) TSCA: Toxic Substances Control Act (USA) WHMIS: National Product Release Inventory (Canada) DOT: US Department of Transportation IATA: International Air Transport Association GHS: Globally Harmonized System of Classification and Labeling of Chemicals ACGIH: American Conference of Governmental Industrial Hygienists CAS: Chemical Abstracts Service (Division of the American Chemical Society) NFPA: National Fire Protection Association (USA)</p>	

54 Created by Global Safety Management, Inc. No. 1-800-425-5181 www.gsmusa.com

Safety Data Sheet	
according to 28CFR16101230 and GHS Rev. 3	
Effective date: 01.08.2015	Page 9 of 8
Hydrochloric Acid,ACS	
<p>HMS: Hazardous Materials Identification System (USA)</p> <p>WHMIS: Workplace Hazardous Materials Information System (Canada)</p> <p>DSL: Domestic Substances List (USA/CA)</p> <p>Effective date: 01.08.2015</p> <p>Last updated: 03.20.2015</p>	

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ATTACHMENT K

Fugitive Emissions Data Summary Sheet

02

Attachment K

FUGITIVE EMISSIONS DATA SUMMARY SHEET

The FUGITIVE EMISSIONS SUMMARY SHEET provides a summation of fugitive emissions. Fugitive emissions are those emissions which could not reasonably pass through a stack, chimney, vent or other functionally equivalent opening. Note that uncontrolled process emissions are not typically considered to be fugitive, and that they are reported on the appropriate EMISSIONS UNIT DATA SHEET and on the EMISSIONS POINTS DATA SUMMARY SHEET. Please note that total emissions from the source are equal to all worked emissions, all fugitive emissions, plus all other emissions (e.g. unapportioned emissions).

APPLICATION FORM CHECKLIST - FUGITIVE EMISSIONS	
1.) Will there be haul road activities?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No
<input type="checkbox"/> IF YES, then complete the HAUL ROAD EMISSIONS UNIT DATA SHEET.	
2.) Will there be Storage Piles?	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
<input type="checkbox"/> IF YES, complete Table 1 of the NONMETALLIC MINERALS PROCESSING EMISSIONS UNIT DATA SHEET.	
3.) Will there be Liquid Loading/Unloading Operations?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No
<input type="checkbox"/> IF YES, complete the BLKX LIQUID TRANSFER OPERATIONS EMISSIONS UNIT DATA SHEET.	
4.) Will there be operations of air pollutants from Wastewater Treatment Exposure?	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
<input type="checkbox"/> IF YES, complete the GENERAL EMISSIONS UNIT DATA SHEET.	
5.) Will there be Equipment Leaks (e.g. leaks from pumps, compressors, boiler process vessels, pressure relief devices, open-ended valves, haphazard connections, flanges, agitators, cooling towers, etc.?)	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No
<input type="checkbox"/> IF YES, complete the LEAK SOURCE DATA SHEET section of the CHEMICAL PROCESSES EMISSIONS UNIT DATA SHEET.	
6.) Will there be General Clean-up VDC Operations?	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
<input type="checkbox"/> IF YES, complete the GENERAL EMISSIONS UNIT DATA SHEET.	
7.) Will there be any other activities that generate fugitive emissions?	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No
<input type="checkbox"/> IF YES, complete the GENERAL EMISSIONS UNIT DATA SHEET or the most appropriate form.	

If you answered "NO" to all of the items above, it is not necessary to complete the following table. "Fugitive Emissions Summary" to

Page 1 of 2 Revision 077

Inc App Email 12/20/2024

Tuesday, February 6, 2024 1:30 PM



Andrews, Edward S <edward.s.andrews@wv.gov>

Incomplete App Email for Permit App R13-3555A

1 message

Andrews, Edward S <edward.s.andrews@wv.gov>

Wed, Dec 20, 2023 at 2:33 PM

To: Bernard Brown <bbrown@empirede.com>, Farley Wood <fwood@empirede.com>, "Pugh, Katie" <Katie.Pugh@tetrattech.com>

Cc: Beverly D Mckeone <beverly.d.mckeone@wv.gov>, Brian S Tephabock <Brian.S.Tephabock@wv.gov>, Eric Blend <eric.n.blend@wv.gov>

**RE: Application Status: Incomplete
Empire Green Generation
Permit Application No. R13-3555A
Plant ID No. 009-00141**

Mr. Brown:

Your application for a modification permit for a plastic recycling by pyrolysis facility was received by this Division on December 1, 2023, and assigned to the writer for review. Upon initial review of said application, it has been determined that the application as submitted is incomplete based on the following items:

1. Affidavit of Publication of Class I Legal Ad.
2. Discussion of the proposed physical change(s), if applicable, and/or change in the method of operation. Specifically, this discussion needs to either outline or go into detail regarding proposed/suggested changes to the permit, if applicable; type and source(s)/origin of the plastic feedstock going to be process by the facility; any processing/pretearting/sorting going to be conduct on the plastic prior to being introduce into the pyrolysis unit(s), if these preprocessing is going to occur of off-site, it still needs to be identified and discussed; a discussion how the facility will switch back and forth in processing medical waste and plastic feedstock; and a discussion why processing the proposed plastic feedstock is not viewed as waste disposal through incineration in the content of the Clean Air Act and meet the criteria as a fuel(s) within the requirements and procedures of 40 CFR 241 - SOLID WASTES USED AS FUELS OR INGREDIENTS IN COMBUSTION UNITS.
3. Plot plan (Attachment E) needs to be updated to identify emission units and emission points.
4. Attachment J needs to be complete for each emission point.
5. Attachments K and L need to be completed. The potential for leaking equipement (e.g., valves, pumps, compressors, connectors, pressure relief devices) needs to be quantified and documented in these two attachments.
6. Each of the redacted pages that contain confidential business information (CBI) needs to be remarks "redacted copy - claim of confidentiality" in accordance with 45CSR31-3.4.

In addressing issues 2 through 6 needs to be reflective within the redacted application as a single PDF file.

The emissions estimates appear to be identical to the emission estimates for processing medical waste with the same pyrolysis unit. Please review these estimates and revise as necessary and/or justify in detail why the emission will not change given the change in feedstocks.

Please address the above deficiencies in writing by no later than January 16, 2024. Application review will not commence until the application has been deemed to be technically complete. Failure to respond to this request in a timely manner may result in the denial of the application.

Should you have any questions, please contact Ed Andrews at (304) 926-0499 ext. 41244 or reply to this email.

--

Edward Andrews, P.E.
Engineer
WVDEP/Division of Air Quality
304-926-0499 Ext 41244
601 57th Street, SE
Charleston, WV 20304

Parcel Notice 12-5-2023

Wednesday, December 6, 2023 8:03 AM



Andrews, Edward S <edward.s.andrews@wv.gov>

You received a parcel! Please come pick it up

1 message

ilobby@ilobbycloud.com <ilobby@ilobbycloud.com>
To: edward.s.andrews@wv.gov

Tue, Dec 5, 2023 at 10:26 AM



Parcel Pending Pick Up

Shipping Label

Date Received

Tracking #

Site Name



Dec 05, 2023

0077429849

WV Department of
Environmental
Protection

Note: AIR

Mark as picked up

App Submittal 12/1/2023

Wednesday, December 6, 2023 8:00 AM



Andrews, Edward S <edward.s.andrews@wv.gov>

Empire Green Generation Permit Modification Application

1 message

Wood, Katie <Katie.Pugh@tetrattech.com>
To: Edward Andrews <edward.s.andrews@wv.gov>
Cc: Farley R Wood <fwood@empirede.com>

Fri, Dec 1, 2023 at 4:09 PM

Ed,


Please find attached Empire Green Generations (EGG) permit modification application attached. EGG is making a claim for confidentiality so the attached file is redacted and the pages that are confidential will arrive via FedEx next week. Please feel free to reach out to me with any questions or concerns.

Thank you,

Katie Wood* | Environmental Scientist
Direct **+1 (740) 298-9062** | Mobile **+1 (304) 559-9980** | katie.wood@tetrattech.com
Formerly Katie Pugh, please note name change
Tetra Tech | *Leading with Science®* | OGA
47443 National Rd Suite 3 | St. Clairesville, OH 47443 | tetrattech.com

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 **R13-3555 Modification_Application_EGG - Redacted_Final 12-1-23.pdf**
21661K